

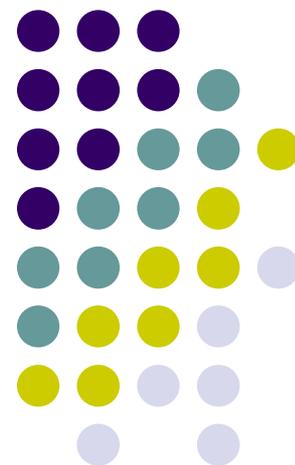
5G NR 實體層技術

Physical Layer Techniques for the 5G New Radio

上課教材



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本上課教材分3大部分

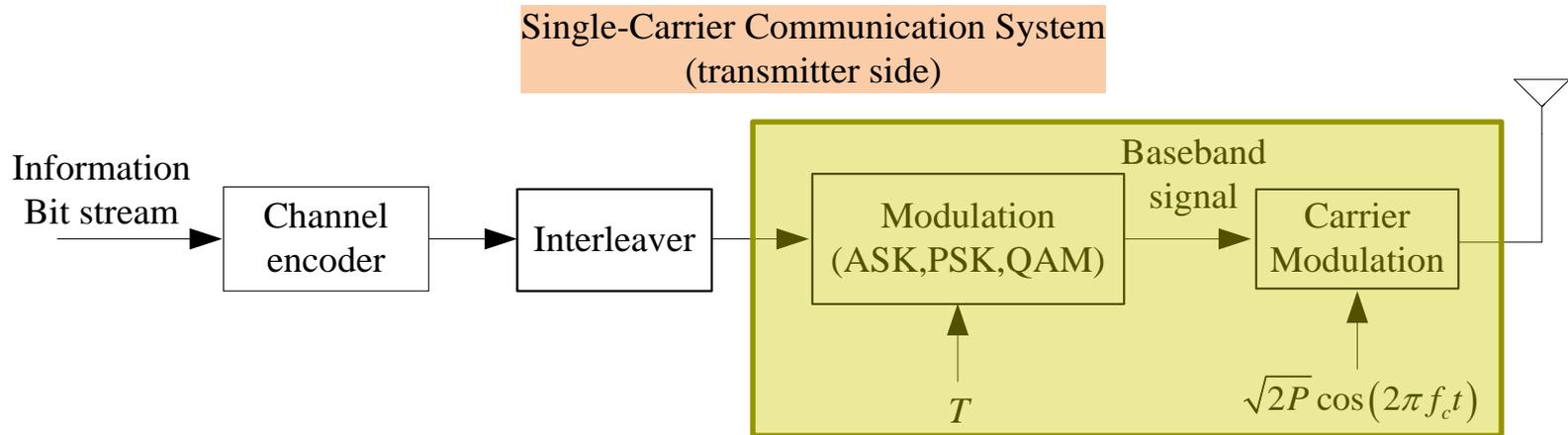
- Part I : Cyclic Prefix Orthogonal Frequency Division Multiplexing (CP-OFDM)
- Part II : New Multi-Carrier Waveforms
 - Universal Filter Multi-Carrier Waveform
 - Filter Bank Multi-Carrier Waveform
 - Generalized Frequency Division Multiplexing
- Part III : Non-Orthogonal Multiple Access (NOMA) Techniques
 - Power-Domain Non-Orthogonal Multiple Access
 - Sparse Code Multiple Access



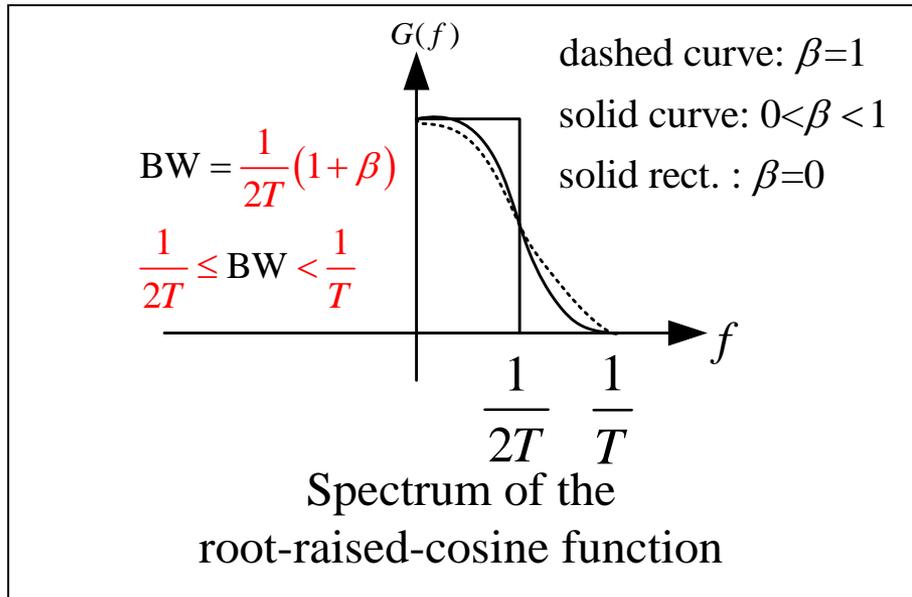
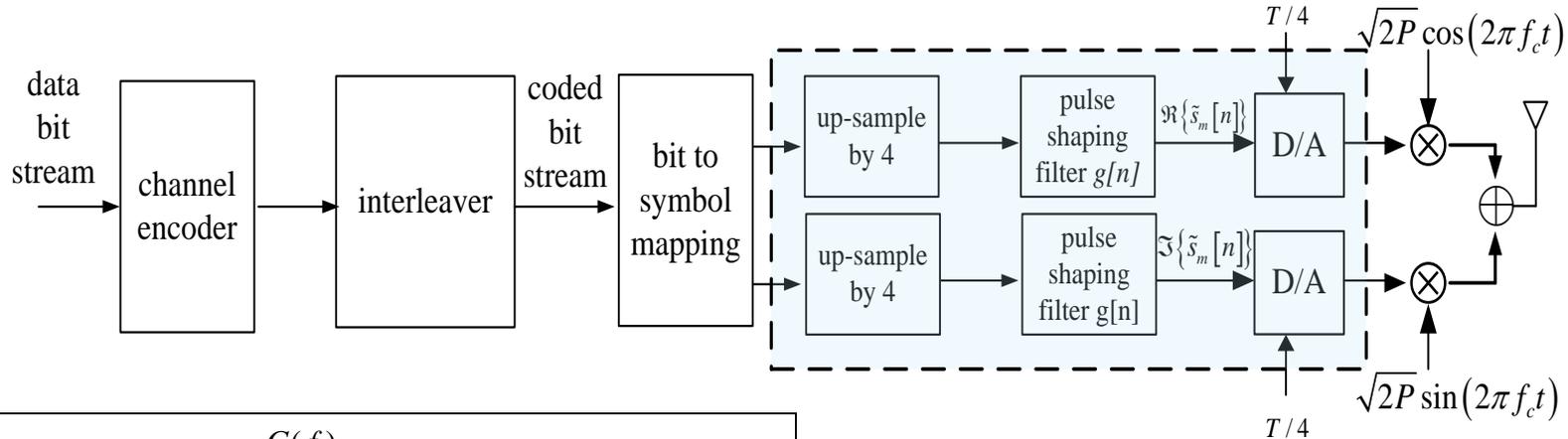
Part I :

Cyclic Prefix Orthogonal Frequency Division Multiplexing (CP-OFDM)

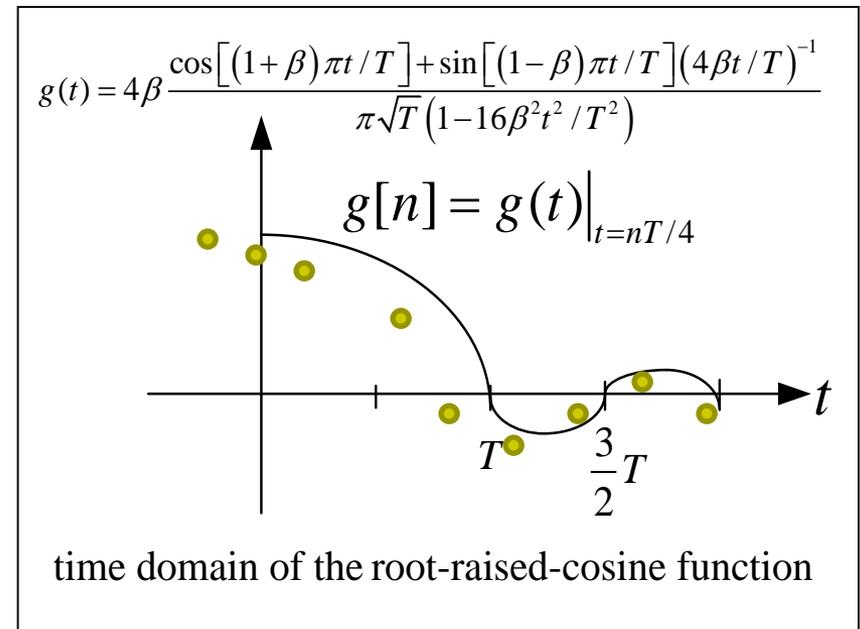
Single-Carrier Communication System



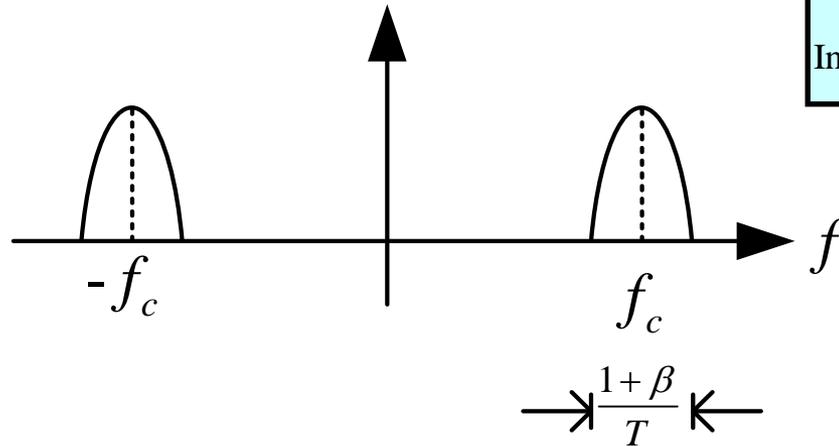
Single Carrier Communication System (1/2)



Baseband bandwidth $\frac{1+\beta}{2T}$



Single Carrier Communication System (2/2)

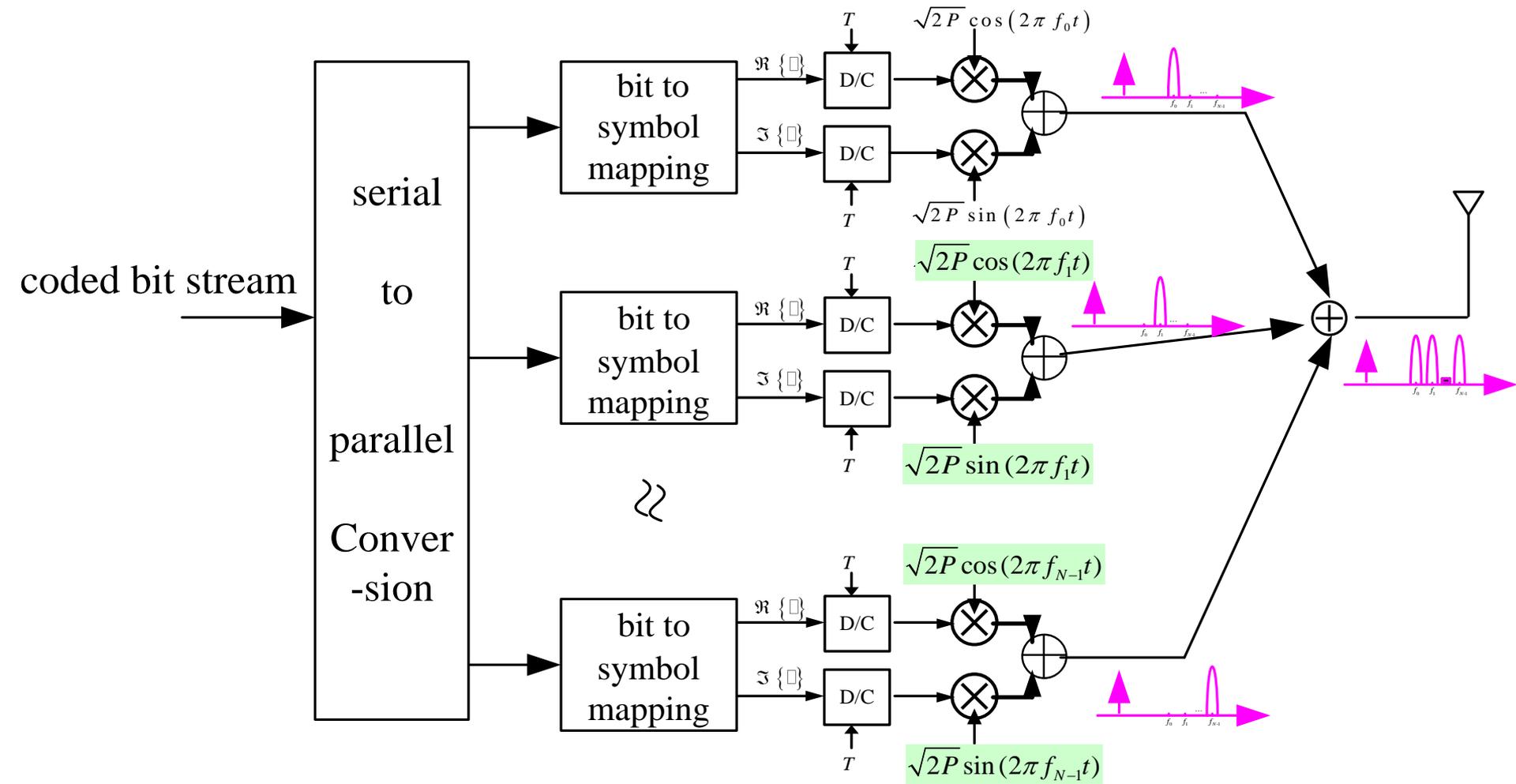


The RF bandwidth is $\frac{1+\beta}{T}$, $0 < \beta < 1$.

In the following, assume $\beta = 0$ and RF BW $\frac{1}{T}$.

| Modulation type | Bits per symbol | Symbols per sec/Hz | bps/Hz |
|-----------------|-----------------|--------------------|--------|
| BPSK | 1 | 1 | 1 |
| QPSK | 2 | 1 | 2 |
| 16-QAM | 4 | 1 | 4 |
| 64-QAM | 6 | 1 | 6 |

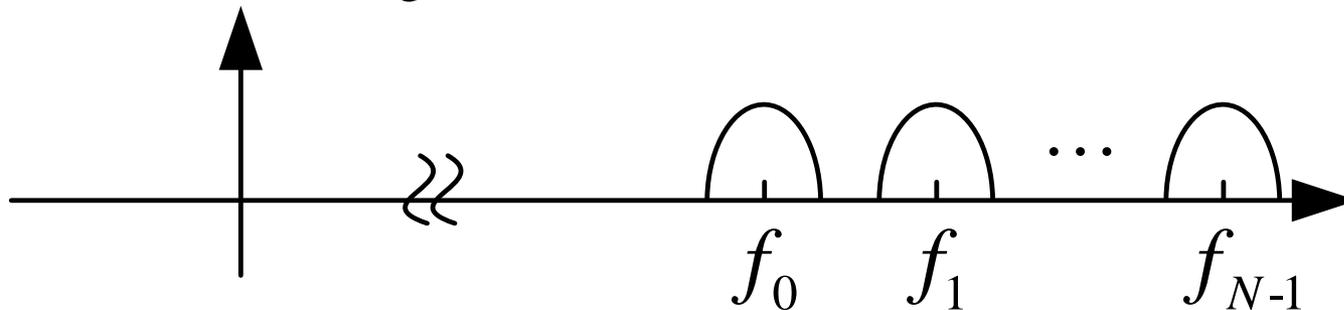
Multi-Carrier Communication System (1/2)



Multi-Carrier Communication System (2/2)

- ◆ If the $f_k, \forall k$, are far apart, the spectrum of the transmitted signal looks as follows.

Spectrum of the multi-carrier modulated signal

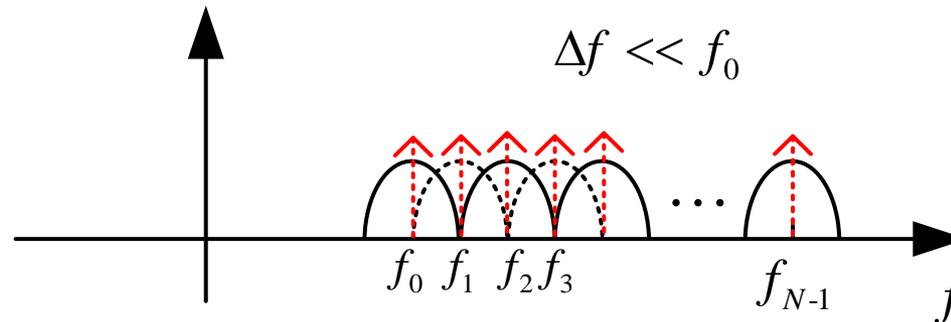


- ◆ The carrier frequencies $f_k, \forall k$, are selected to **avoid spectrum overlapping** such that modulated signals associated with all carriers do not interfere with one another.

The OFDM System (1/3)

- ◆ **However**, if the carrier frequencies satisfy $f_k = f_0 + k\Delta f$, $k = 0, \dots, N-1$ where f_0 and $\Delta f = \frac{1}{T}$ are fixed values, the spectrum looks like

The spectrum of all multiple carrier modulated signals



The spectra of all multiple sub-signals are **overlapped**.

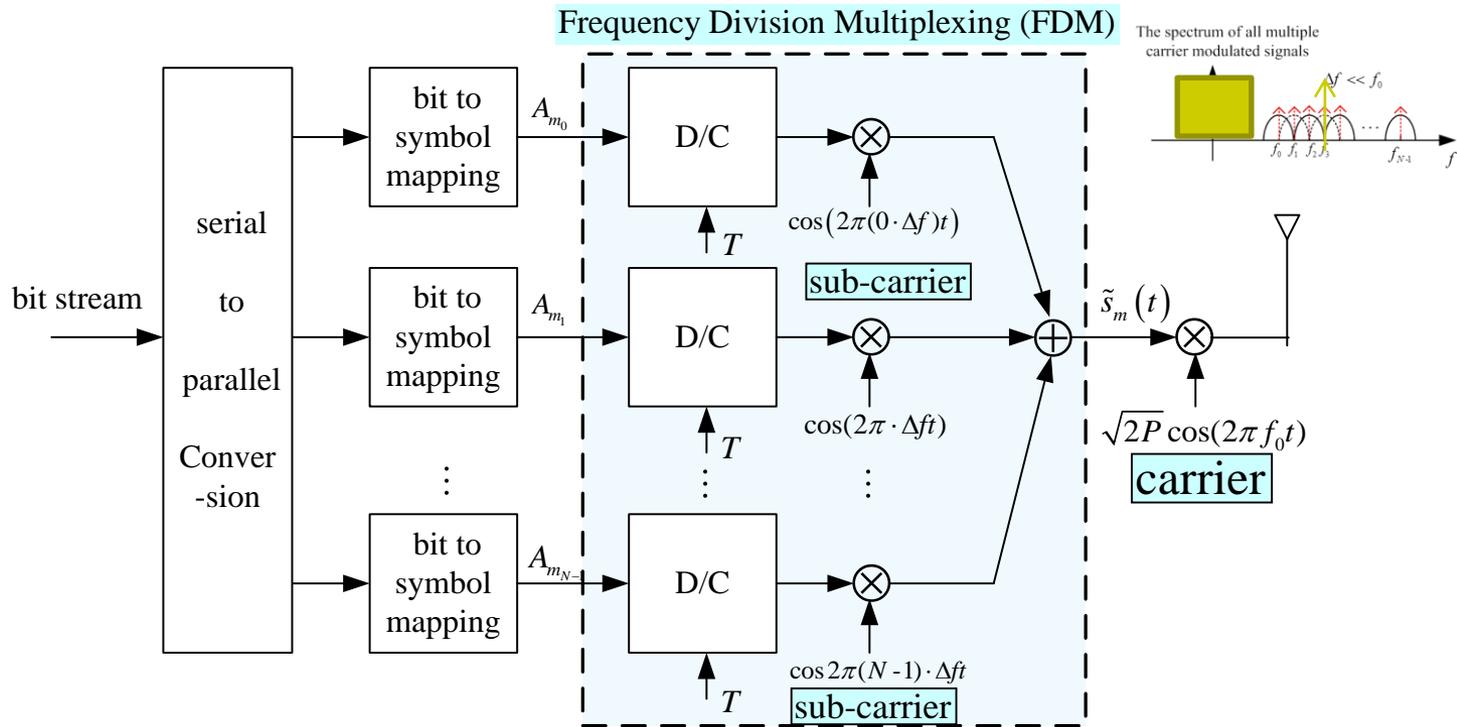
It appears that the multiple sub-signals may interfere with one another.

However, the frequency components at **frequency instants** $f_k = f_0 + k\Delta, \forall k$, do not interfere with one another.

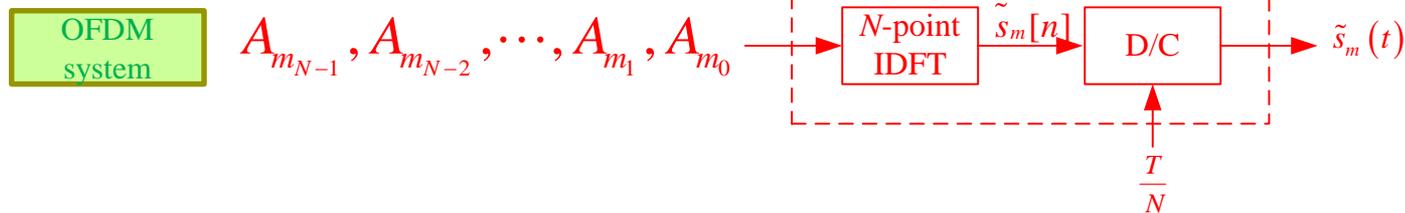
Through **precise frequency synchronization**, the receiver can obtain through accurate sampling the frequency components at these frequency instants.

Hence, transmitting signal by this scheme requires accurate frequency synchronization.

The OFDM System (2/3)



Implemented by IDFT



The N sub-carriers $\{\cos(0 \cdot 2\pi \Delta f t), \cos(1 \cdot 2\pi \Delta f t), \dots, \cos((N-1) \cdot 2\pi \Delta f t)\}$ are **orthogonal**.

The IDFT in OFDM plays **digitally** the role of FDM as in the multi-carrier communication system. 10

The OFDM System (3/3)

- ◆ The OFDM system is a structure of **Orthogonal FDM** of N parallel signal streams.

- ◆ Advantages of the OFDM system over the multi-carrier (MC)-system:
 - **High spectral efficiency (two-fold)**
 - Low-complexity (1-tapped) channel equalization
 - **Only one RF chain (one mixer/power amplifier, one high-speed DAC)**
 - **Cheap and stable digital FFT to implement the Orthogonal FDM**

Subcarrier Modulation Mapping (1/2)

- The encoded and interleaved binary serial input data shall be divided into **groups** of N_{BPSC} (1, 2, 4, or 6) bits and converted into **complex numbers** representing BPSK, QPSK, 16-QAM, or 64-QAM constellation points.
- The output values, d , are formed by multiplying the resulting $(I + jQ)$ value by a normalization factor K_{MOD} , as follow

$$d = (I + jQ) \times K_{MOD}.$$

Table 82 - BPSK encoding table

| Input bit (b0) | I-out | Q-out |
|----------------|-------|-------|
| 0 | -1 | 0 |
| 1 | 1 | 0 |

Table 81 - Modulation-dependent normalization factor K_{MOD} to make $E\{|d|^2\} = 1$.

| Modulation | K_{MOD} |
|------------|---------------|
| BPSK | 1 |
| QPSK | $1/\sqrt{2}$ |
| 16-QAM | $1/\sqrt{10}$ |
| 64-QAM | $1/\sqrt{42}$ |



Subcarrier Modulation Mapping (2/2)

Table 83 - QPSK encoding table b_0b_1

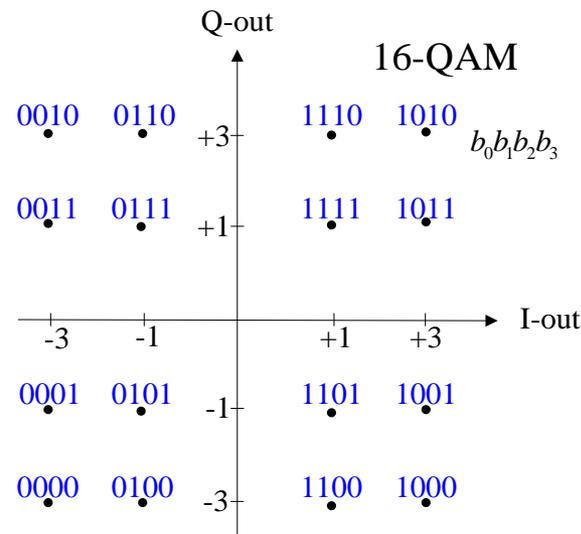
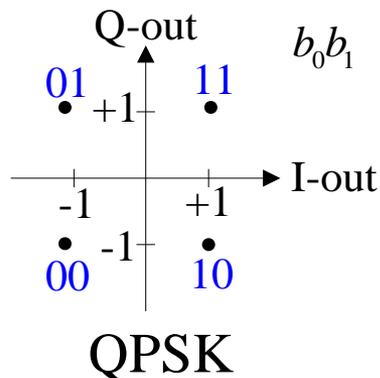
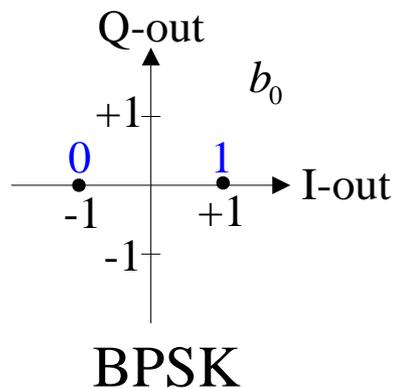
| Input bit (b0) | I-out | Input bit (b1) | Q-out |
|----------------|-------|----------------|-------|
| 0 | -1 | 0 | -1 |
| 1 | 1 | 1 | 1 |

Table 84 - 16-QAM encoding table $b_0b_1b_2b_3$

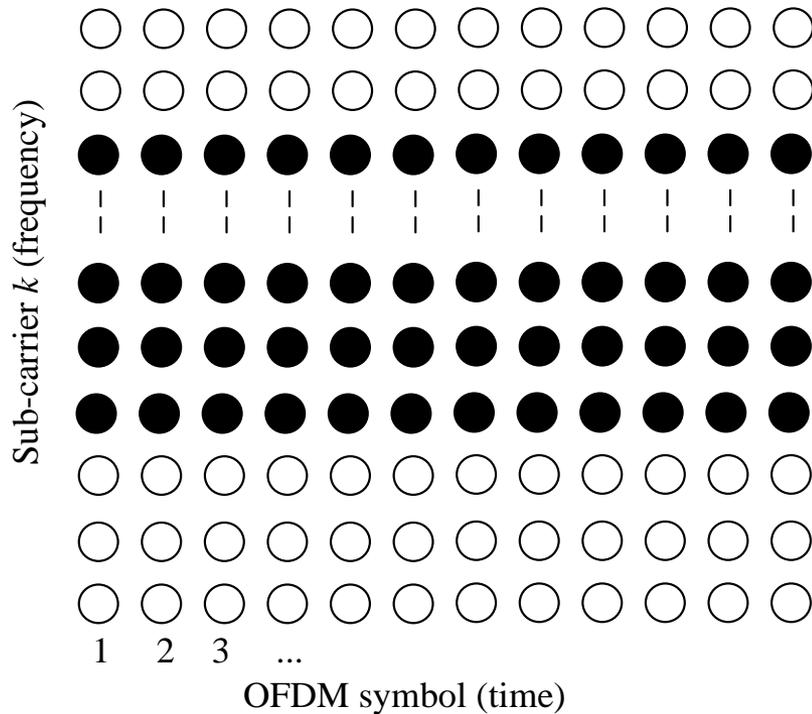
| Input bits (b0 b1) | I-out | Input bits (b2 b3) | Q-out |
|--------------------|-------|--------------------|-------|
| 00 | -3 | 00 | -3 |
| 01 | -1 | 01 | -1 |
| 11 | 1 | 11 | 1 |
| 10 | 3 | 10 | 3 |

Table 85 - 64-QAM encoding table $b_0b_1b_2b_3b_4b_5$

| Input bits (b0 b1 b2) | I-out | Input bits (b3 b4 b5) | Q-out |
|-----------------------|-------|-----------------------|-------|
| 000 | -7 | 000 | -7 |
| 001 | -5 | 001 | -5 |
| 011 | -3 | 011 | -3 |
| 010 | -1 | 010 | -1 |
| 110 | 1 | 110 | 1 |
| 111 | 3 | 111 | 3 |
| 101 | 5 | 101 | 5 |
| 100 | 7 | 100 | 7 |



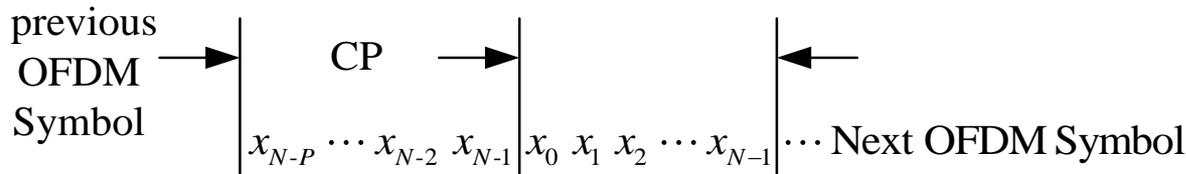
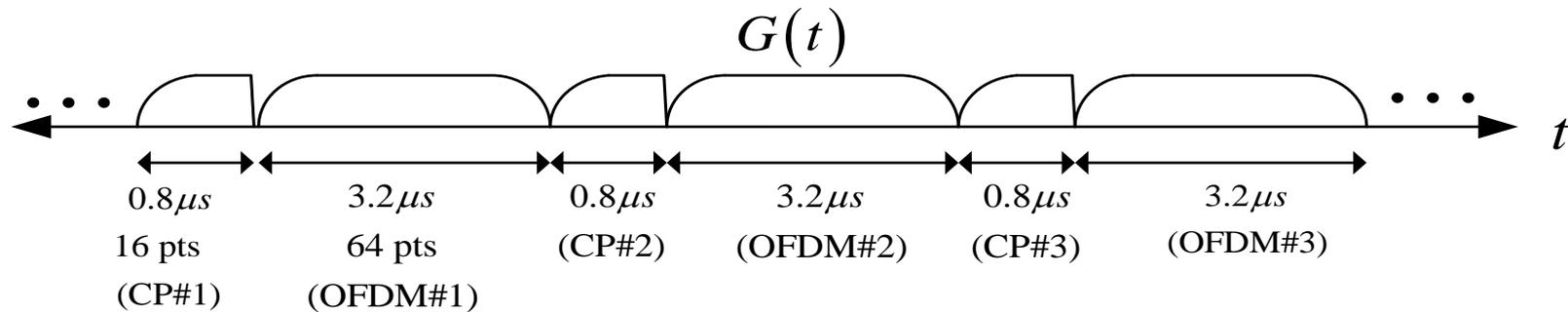
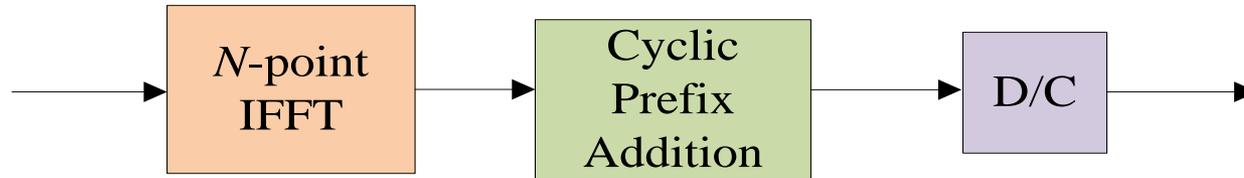
Time-Frequency Representation



- Each black/white dot represents a sub-carrier symbol.
- One OFDM symbol is comprised of N (modulated) symbols.
- The N symbols are transmitted over a OFDM symbol duration of T seconds.

- The **inter-subcarrier spacing** is equal to $1/T$ Hz.
- The sampling rate is $1/(NT)$ Hz.

Cyclic Prefix for OFDM



One OFDM symbol may include:

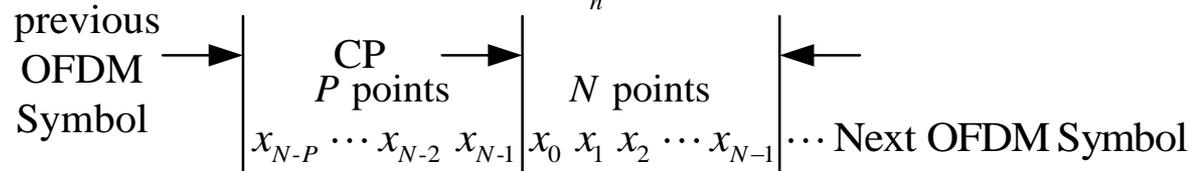
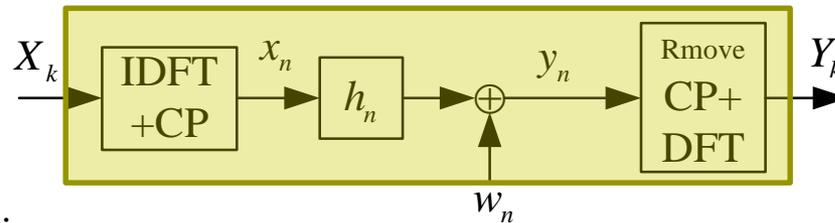
N symbols (data in frequency domain)

N samples (IFFT size in both time and frequency domains)

$N + P$ samples (IFFT size plus CP length in time domain)

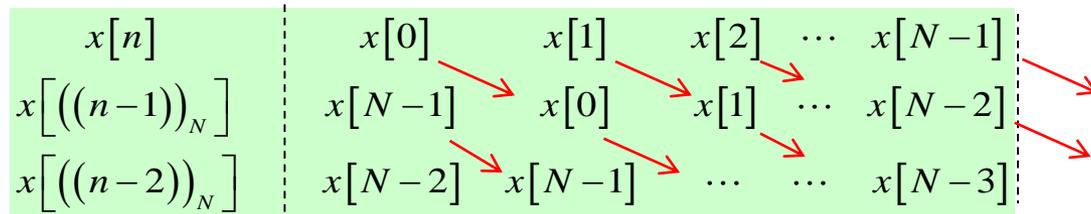
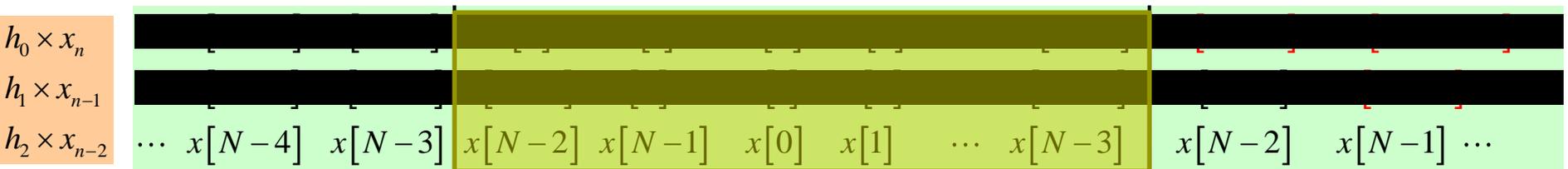
Why is CP used ? (1/3)

◆ Consider the following system



$$y_n = \sum_{k=0}^{L-1} x_{n-k} h_k + w_n = h_0 x_n + h_1 x_{n-1} + \dots + h_{L-1} x_{n-L+1} + w_n$$

y[0] y[1] y[2] y[3] ... y[N-1]



Why is CP used ? (2/3)

$$\underbrace{\begin{bmatrix} y_0 \\ y_1 \\ \vdots \\ \vdots \\ \vdots \\ y_{N-1} \end{bmatrix}}_{\mathbf{y} \quad N \times 1} = \underbrace{\begin{bmatrix} x_0 & x_{N-1} & x_{N-2} & \cdots & x_1 \\ x_1 & x_0 & x_{N-1} & \cdots & x_2 \\ \vdots & & \ddots & & \vdots \\ x_{N-1} & x_{N-2} & \cdots & \cdots & x_0 \end{bmatrix}}_{\mathbf{x} \quad N \times N} \underbrace{\begin{bmatrix} h_0 \\ \vdots \\ h_{L-1} \\ 0 \\ \vdots \\ 0 \end{bmatrix}}_{\mathbf{h} \quad N \times 1} + \underbrace{\begin{bmatrix} w_0 \\ w_1 \\ \vdots \\ \vdots \\ \vdots \\ w_{N-1} \end{bmatrix}}_{\mathbf{w} \quad N \times 1}$$

circulant matrix

Define the DFT matrix by

$$\mathbf{F} = \frac{1}{\sqrt{N}} \begin{bmatrix} w_N^{00} & \cdots & w_N^{0 \cdot (N-1)} \\ \vdots & & \vdots \\ w_N^{(N-1) \cdot 0} & \cdots & w_N^{(N-1) \cdot (N-1)} \end{bmatrix}_{N \times N}, \text{ where } w_N = e^{-j2\pi \frac{nk}{N}}$$

$$\mathbf{F}\mathbf{F}^H = \mathbf{F}^H\mathbf{F} = \mathbf{I}$$

Then,

$$\underbrace{\mathbf{F}\mathbf{y}}_{\mathbf{y}} = \underbrace{\mathbf{F}\mathbf{x}}_{\mathbf{x}} \underbrace{\mathbf{F}^H}_{\mathbf{H}} \underbrace{\mathbf{F}\mathbf{h}}_{\mathbf{H}} + \underbrace{\mathbf{F}\mathbf{w}}_{\mathbf{w}}$$

Why is CP used ? (3/3)

- ◆ Note that

$$\underbrace{\begin{bmatrix} Y_0 \\ Y_1 \\ \vdots \\ Y_{N-1} \end{bmatrix}}_{\mathbf{Y}} = \underbrace{\begin{bmatrix} X_0 & 0 & \cdots & 0 \\ 0 & X_1 & 0 & \vdots \\ \vdots & 0 & \ddots & 0 \\ 0 & \cdots & 0 & X_{N-1} \end{bmatrix}}_{\mathbf{X}} \underbrace{\begin{bmatrix} H_0 \\ H_1 \\ \vdots \\ H_{N-1} \end{bmatrix}}_{\mathbf{H}} + \underbrace{\begin{bmatrix} W_0 \\ W_1 \\ \vdots \\ W_{N-1} \end{bmatrix}}_{\mathbf{W}}$$

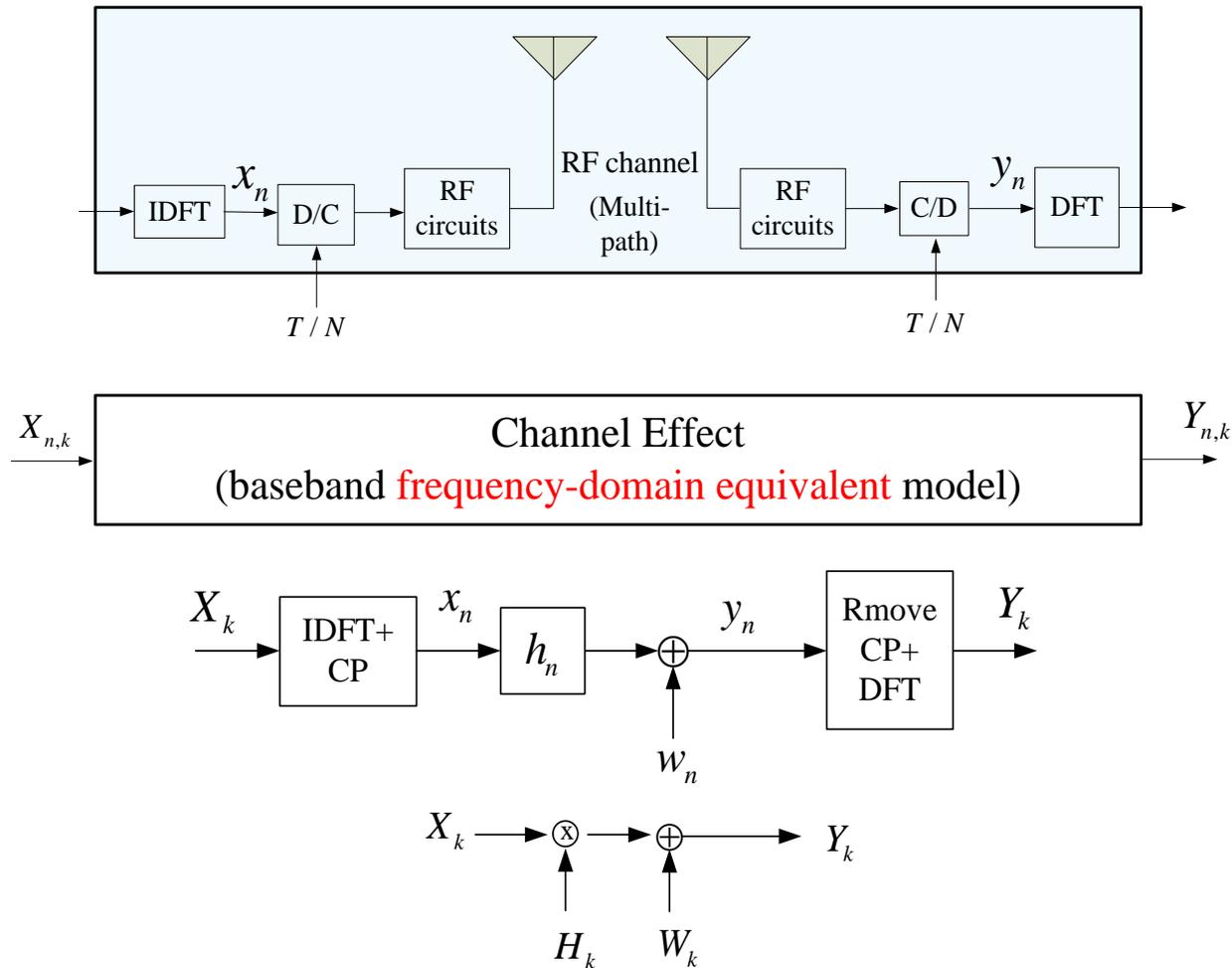
- ◆ It must be satisfied that $P \geq L$ to avoid ISI.
- ◆ It is essential to prove that $\mathbf{F}\mathbf{x}\mathbf{F}^H$ is diagonal.
- ◆ The above frequency-domain model can be written as

$$Y_k = X_k H_k + W_k, \quad k = 0, 1, \dots, N-1$$

k is the sub-carrier index.

- ◆ The **frequency-selective channel** now becomes **frequency non-selective**.

Complete Channel Effects



The frequency-selective channel now becomes frequency non-selective.

Cyclic Prefix vs Guard Time

| Guard Time | Cyclic Prefix |
|---|--|
| Eliminates Inter-symbol Interference | Eliminates Inter-symbol Interference |
| Suffers from Inter-carrier Interference | Eliminates Inter-carrier Interference |
| Suffers from Intra-carrier Interference | Suffers from Intra-carrier Interference |
| Causes a reduction in data rate as a result of the increased OFDM symbol time | Causes a reduction in data rate as a result of the increased OFDM symbol time |
| Does not consume additional power associated with OFDM symbol time expansion due to the guard time | Necessitates additional power associated with OFDM symbol expansion due to the introduction of cyclic prefix |

Pulse Shaping and Spectrum Mask

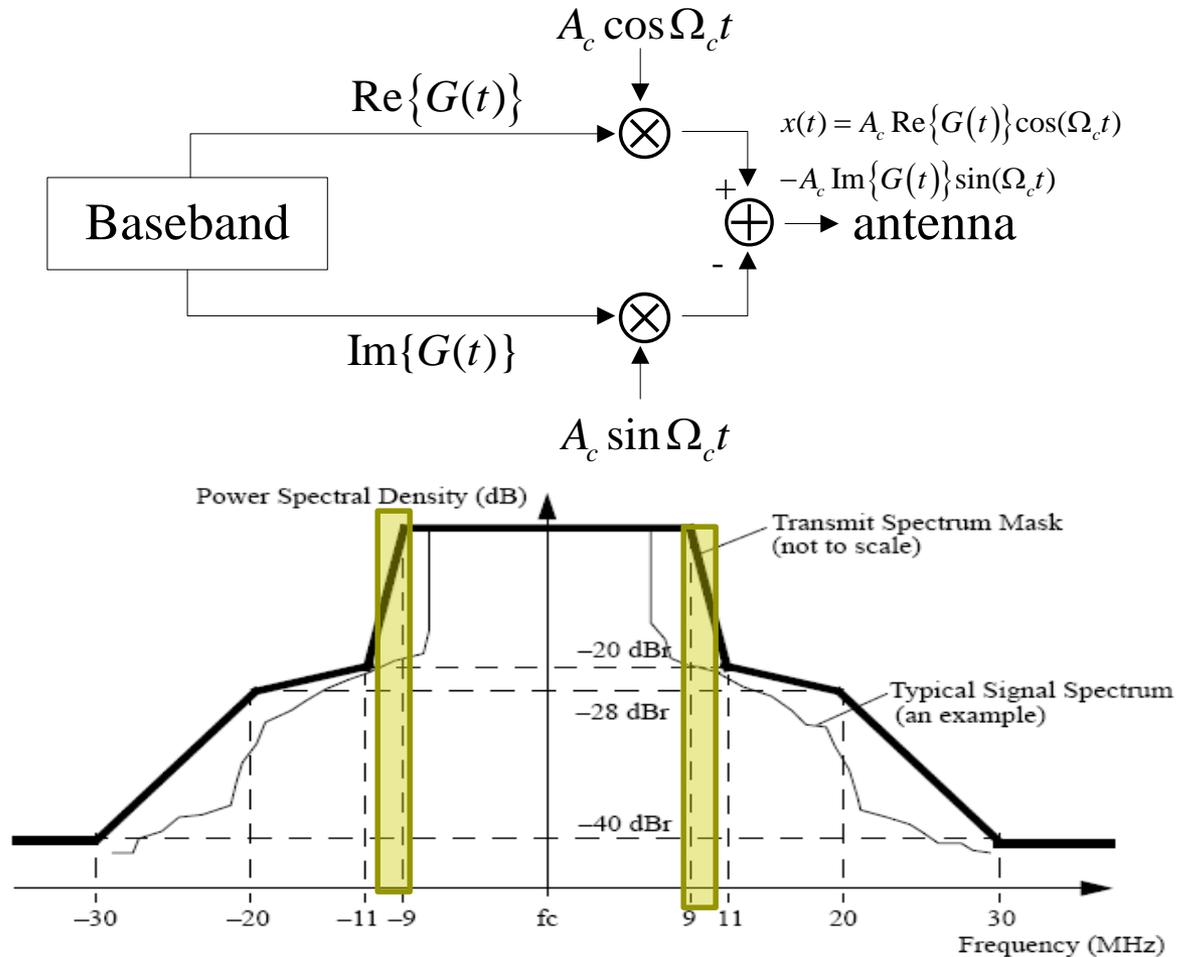
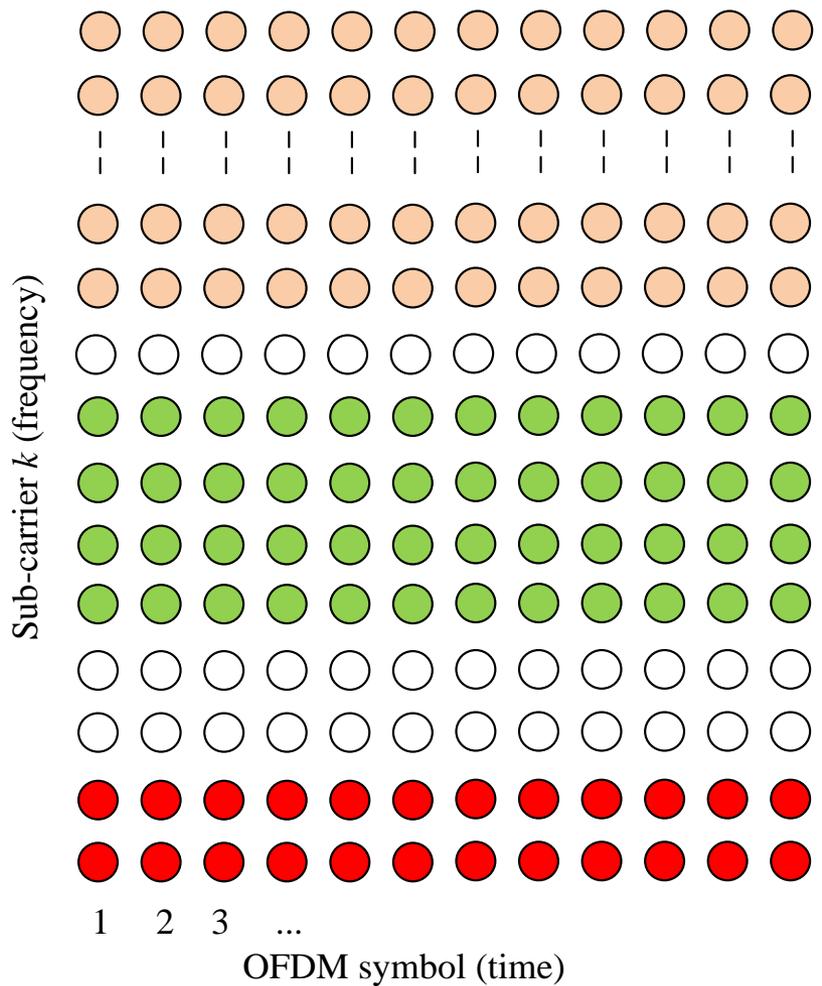


Figure 120—Transmit spectrum mask

Baseband bandwidth W :

subcarrier #26 = $27 \times 312.5 \text{ KHz} = 8.4375 \text{ MHz}$ or $32 \times 312.5 \text{ KHz} = 10 \text{ MHz}$ 21

Orthogonal Frequency Division Multiple Access (OFDMA)



➤ Each user is allocated with a fixed number of sub-carriers

Physical Layer Parameters for LTE

| Channel Bandwidth (MHz) | 1.4 | 3 | 5 | 10 | 15 | 20 |
|--|---|-------|-------|-------|--------|--------|
| Frame Duration (ms) | 10 | 10 | 10 | 10 | 10 | 10 |
| Sub carrier spacing (Khz) | 15 | 15 | 15 | 15 | 15 | 15 |
| Sampling Frequency (Mhz) | 1.92 | 3.84 | 7.68 | 15.36 | 23.04 | 30.72 |
| FFT Size | 128 | 256 | 512 | 1024 | 1536 | 2048 |
| Occupied Subcarriers (including DC) | 73 | 181 | 301 | 601 | 901 | 1201 |
| Guard Subcarriers | 55 | 75 | 211 | 423 | 635 | 847 |
| Number of Resource Blocks | 6 | 15 | 25 | 50 | 75 | 100 |
| Occupied Channel Bandwith (Mhz) | 1.095 | 2.715 | 4.515 | 9.015 | 13.515 | 18.015 |
| DL Bandwidth Efficiency | 78.2% | 90% | 90% | 90% | 90% | 90% |
| OFDM Symbols for Subframe (for Short CP) | 7 | 7 | 7 | 7 | 7 | 7 |
| CP Length for Short CP (in us) | 5.2 for the first symbol/4.69 for other symbols | | | | | |



Advantages of CP-OFDM

- ◆ The OFDM spectrum is composed of overlapped narrow subcarriers. This makes efficient usage of frequency spectrum compared to traditional FDM method.
- ◆ The OFDM broadband channel is divided into smaller narrowband subchannels. This makes OFDM resistive to frequency selective fading. Moreover OFDM transmit/receive chain uses channel encoder/decoder and interleaver/deinterleaver which help in recovering lost OFDM symbols due to fading.
- ◆ OFDM makes use of cyclic prefix to eliminate ISI (Inter Symbol Interference) found in the multipath channel environment. Hence it is robust to multipath fading.
- ◆ Channel estimation and equalization has been carried out using known pattern (i.e. preamble) and embedded pilot carriers in a symbol. This is more simpler and efficient compare to channel equalization used in to SC (Single Carrier) system.
- ◆ Time offset estimation and correction algorithms are very easy due to correlation technique.
- ◆ It is possible to allocate bandwidth as per resource requirements. Hence OFDM is bandwidth scalable technique.



Disadvantages of CP-OFDM

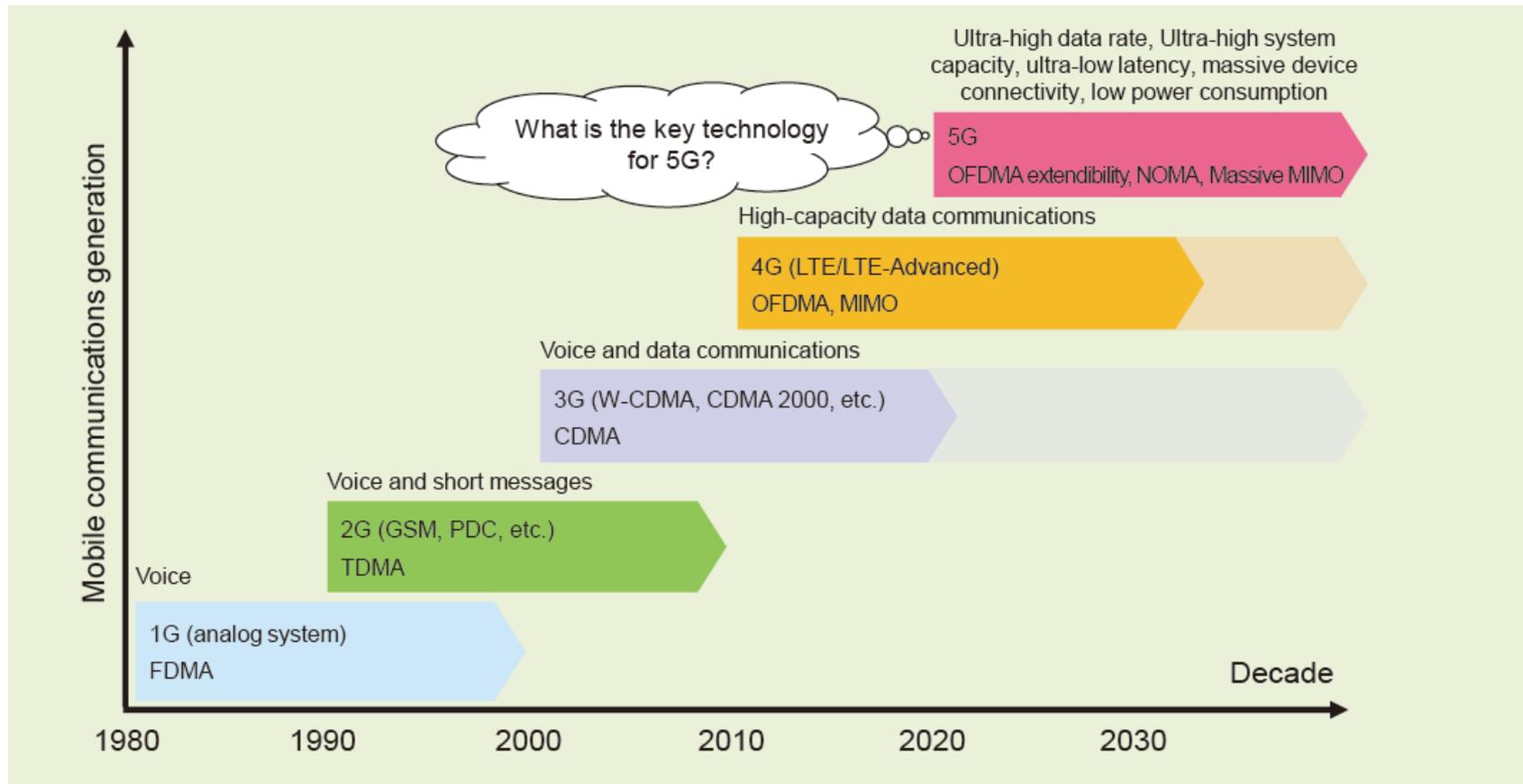
- ◆ OFDM signal spectrum has higher peak to average power ratio (PAPR). Due to this, OFDM based transmission system requires radio frequency power amplifier (PA) with higher PAPR.
- ◆ It has higher carrier frequency offset due to different LOs (Local Oscillators) and DFT leakage. This requires complex frequency offset correction algorithms at the OFDM receiver.
- ◆ It is prone to Inter-Symbol Interference (ISI) and Inter-Carrier Interference (ICI). This requires time offset and frequency offset correction algorithms.
- ◆ When OFDM signal travels through multiple paths, guard interval is required to avoid ISI errors due to timing offsets.

Part II :

New Multi-Carrier Waveforms

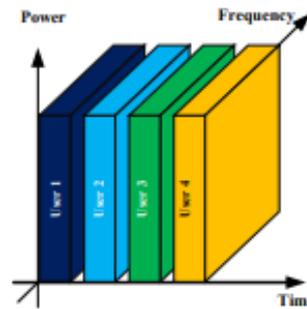
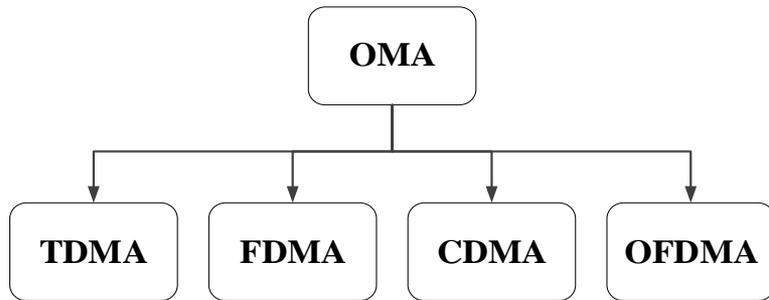
- Universal Filter Multi-Carrier (UFMC) Waveform
- Filter Bank Multi-Carrier (FBMC) Waveform
- Generalized Frequency Division Multiplexing (GFDM) Waveform

The 5G Communication

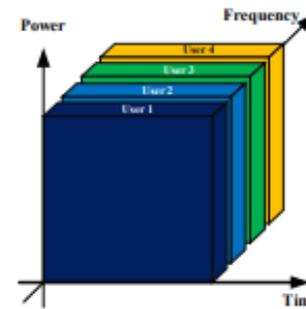


- ◆ **Enhanced Mobile Broadband (eMBB)**
- ◆ **Ultra-reliable and Low Latency Communications (URLLC)**
- ◆ **Massive Machine Type Communications (mMTC)**

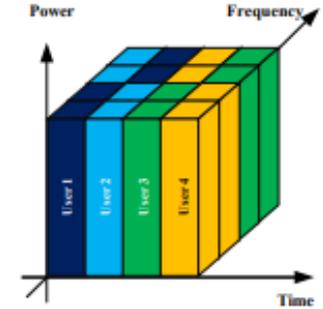
Orthogonal Multiple Access (OMA)



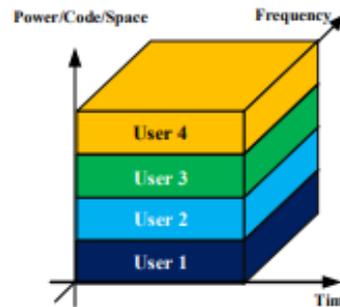
a) TDMA



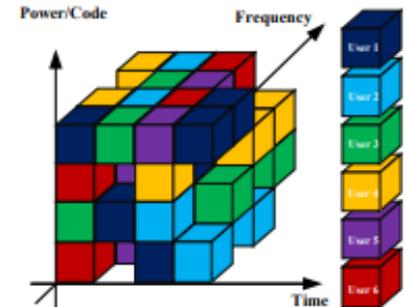
b) FDMA



c) OFDMA



d) CDMA/SDMA



e) Possible NoMA Solution

Y. Chen, A. Bayesteh, Y. Wu, B. Ren, S. Kang, S. Sun, Q. Xiong, C. Qian, B. Yu, Z. Ding, S. Wang, S. Han, X. Hou, H. Lin, R. Visoz, and R. Razavi, "Towards the standardization of non-orthogonal multiple access for next generation wireless networks," IEEE Commun. Mag., vol. 56, no. 3, pp. 19–27, Mar. 2018.

The Problem with CP-OFDM

- While windowing and filtering can indeed **reduce the out-of-band (OOB) emissions** of conventional OFDM, filter bank multicarrier modulation (FBMC) with offset quadrature amplitude modulation (OQAM) still performs much better, as shown in Fig. 3.1.

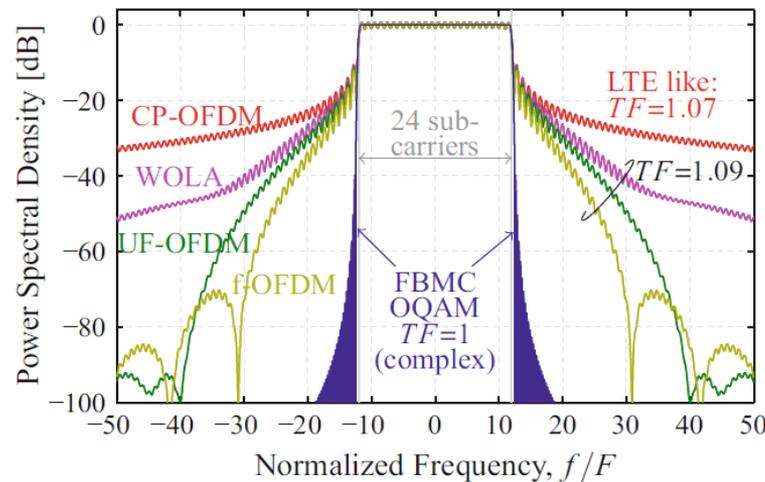


Fig. 3.1 FBMC has much better spectral properties compared with CP-OFDM. Windowing (WOLA) and filtering (UF-OFDM, f-OFDM) can improve the spectral properties of CP-OFDM. However, FBMC still performs much better and has the additional advantage of a maximum symbol density, $TF = 1$ (complex). ©2017 IEEE, [41]

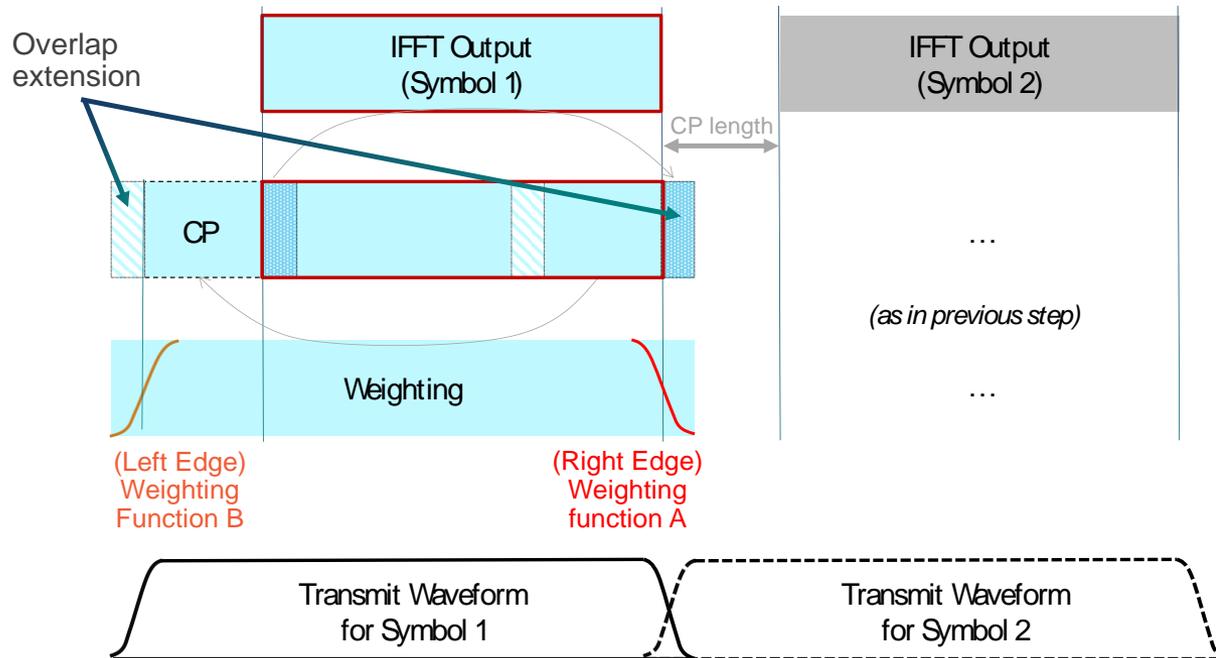
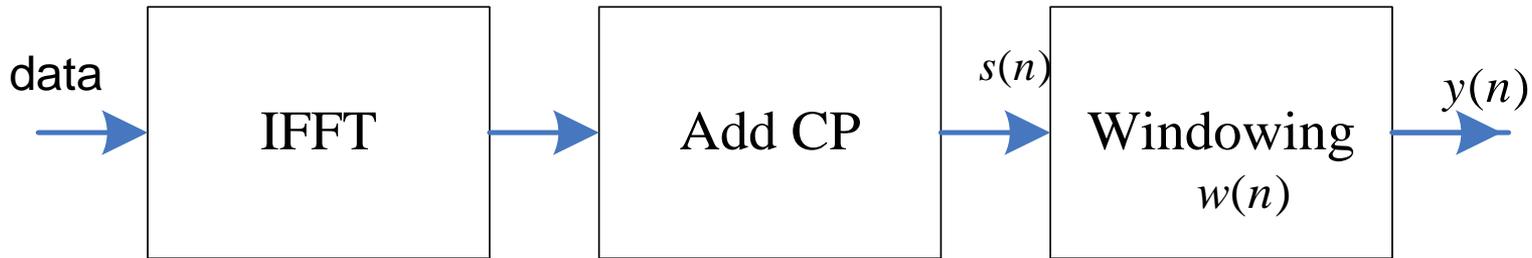
New Waveforms

Table III The summary and comparison of three new waveforms

| Waveforms | Features | Key technologies | Advantages | Disadvantages |
|-----------|----------|-------------------------------------|---|--|
| FBMC | | multi-carrier filtering | (1) the flexible control of the degree of overlap between each sub-carrier (2) time-frequency efficiency improvement by about 10% in case of very short packets (3) low synchronization requirement | (1) large interference between sub-carriers (2) the long filter length, high complexity |
| UFMC | | block-wise filtering | (1) the short filter length, Low complexity (2) time-frequency efficiency improvement by about 10% in any case (3) small interference between sub-carriers | (1) higher synchronization requirement than CP-OFDM |
| GFDM | | Tx-filtering FFT-based equalization | (1) lower PARP (2) use of scattered spectrum resources (3) ultra-low out-of-band radiation | (1) receiver is rather complex |

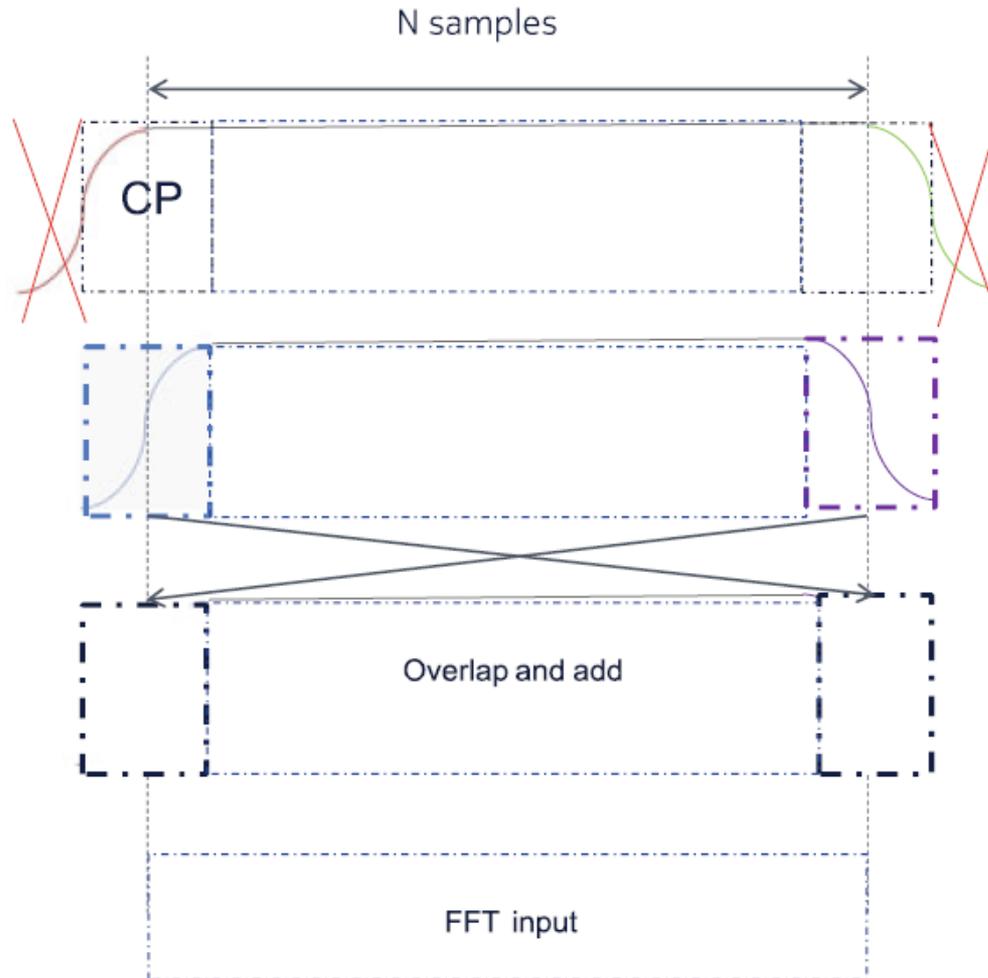
The Universal Filter Multi-Carrier (UFMC) Waveform

CP-OFDM with Weighted Overlap and Add (WOLA) (1/2)



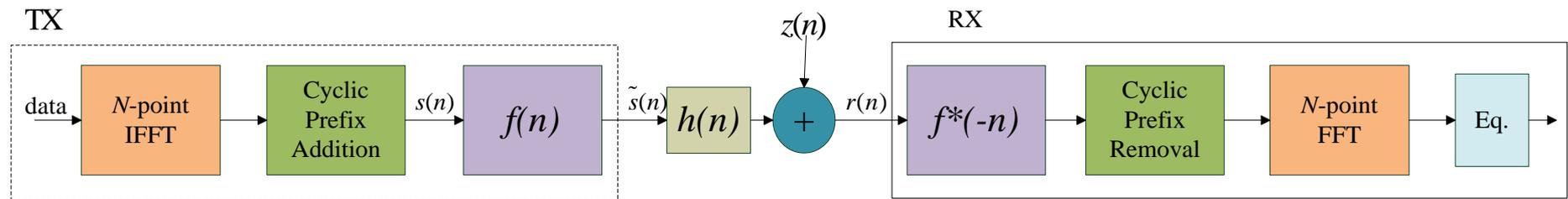
$$y(n) = s(n) \cdot w(n)$$

CP-OFDM with Weighted Overlap and Add (WOLA) (2/2)



R. Zayani, Y. Medjahdi, H. Shaiek, and D. Roviras, "WOLA-OFDM: A Potential Candidate for Asynchronous 5G," in *Proc. IEEE Globecom Workshops (GC Wkshps)*, Feb. 2017, pp. 1-5.

Filtered-OFDM (1/3)



- ◆ Filtered OFDM (f-OFDM) is a 5G candidate waveform based on **sub-band filtering by**

$$f(n) = w(n)p_B(n),$$

where $p_B(n)$ is a sinc impulse response with **bandwidth B** in the frequency domain equal to the sub-band allocation size.

Also $w(n)$ over duration $T_w = \frac{T_u}{2}$ is the windowing mask to have smooth transitions.

- ◆ For practical implementation, the sine function is soft-truncated with different window functions:

1. Hanning window

$$w(t) = \begin{cases} 0.5[1 + \cos(2\pi |t|/T_w)], & |t| \leq \frac{T_w}{2} \\ 0, & |t| > \frac{T_w}{2} \end{cases}$$

2. Root-raised-cosine (RRC) window

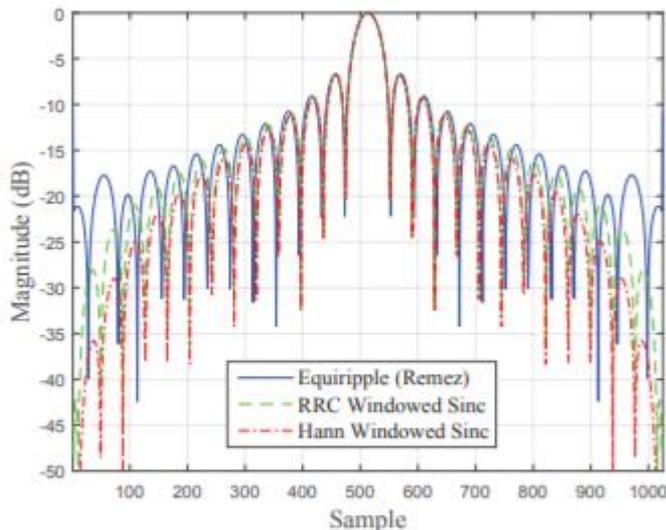


Figure 4. Impulse response of different filters.

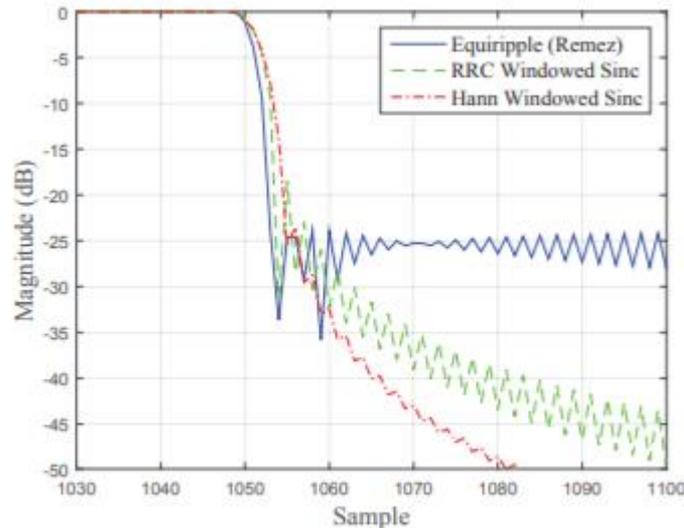
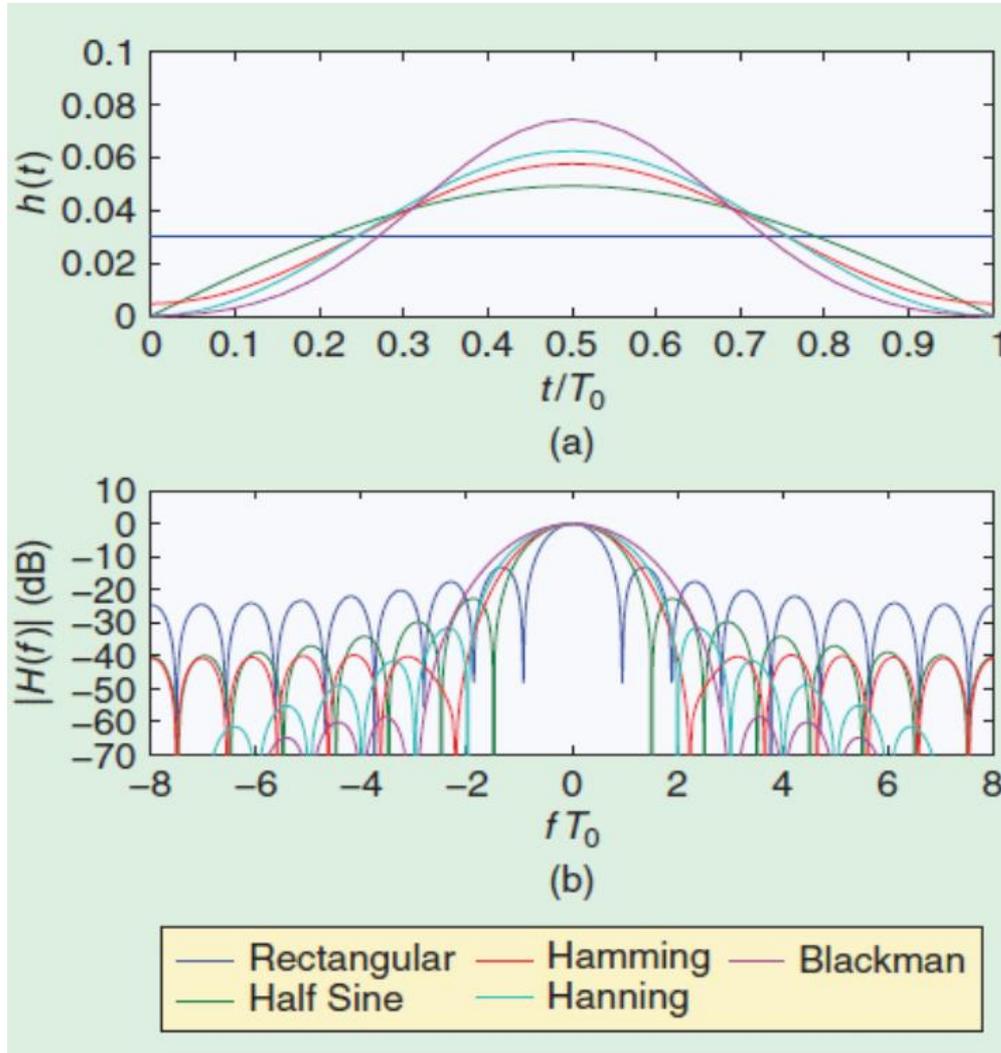


Figure 5. Frequency response of different filters.

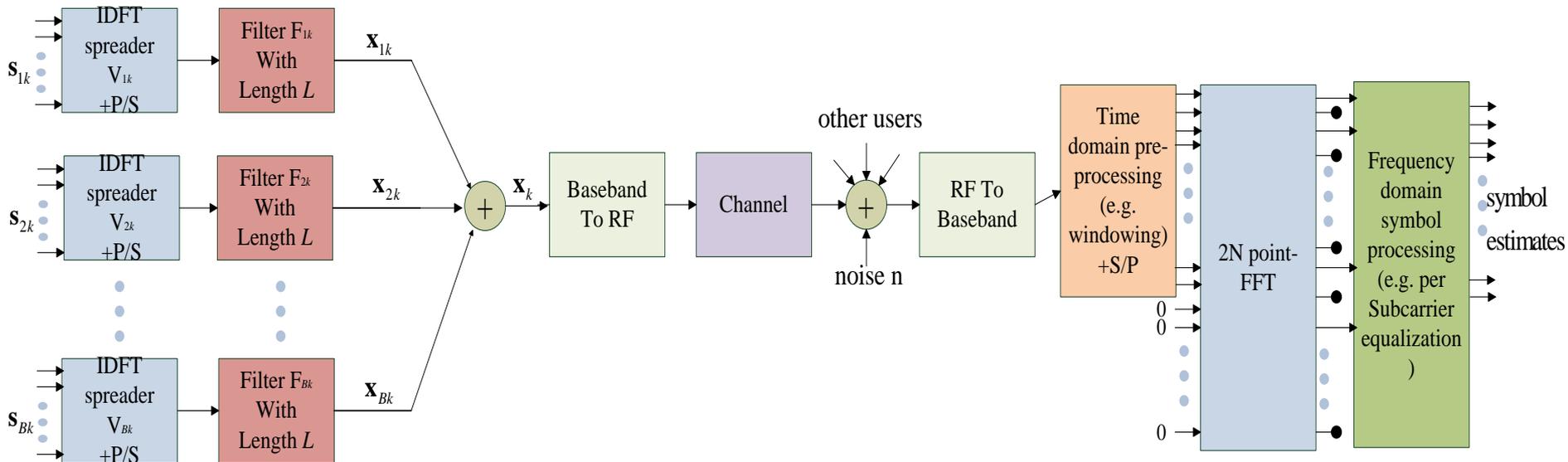
Filtered-OFDM (3/3)



Hamming, Hanning, and Blackman windows offer lower side lobes at the cost of a wider main lobe.

Universal Filtered Multi-Carrier (UFMC) (1/5)

- ◆ UF-OFDM is a 5G candidate waveform, also known as universal filtered-multi-carrier (UFMC), where **blocks of subcarriers (sub-bands)** are filtered.



Universal Filtered Multi-Carrier (UFMC) (2/5)

- ◆ IFFT symbols are generated in the same way as legacy CP-OFDM. Instead of CP, **a guard interval (GI)** filled with zeros is introduced between the IFFT symbols to prevent ISI due to transmit filter delay.
- ◆ **Dolph–Chebychev filters are optimal in the sense that for a given side lobe level (SLL) the main lobe width is minimized.** They are adjustable by the tuning parameter for the **side lobe attenuation (SLA)** as well as by the filter length N .

$$W(k) = \frac{\cos \left\{ N \cos^{-1} \left[\beta \cos \left(\frac{\pi k}{N} \right) \right] \right\}}{\cosh \left[N \cosh^{-1}(\beta) \right]}, \quad k = 0, 1, 2, \dots, N-1$$

$$\beta = \cosh \left[\frac{1}{N} \cosh^{-1} \left(10^\alpha \right) \right] \quad \text{with sidelobe in db} = -20\alpha$$

$$w_0(n) = \frac{1}{N} \sum_{k=0}^{N-1} W(k) e^{j2\pi kn/N}, \quad -N/2 \leq n \leq N/2$$

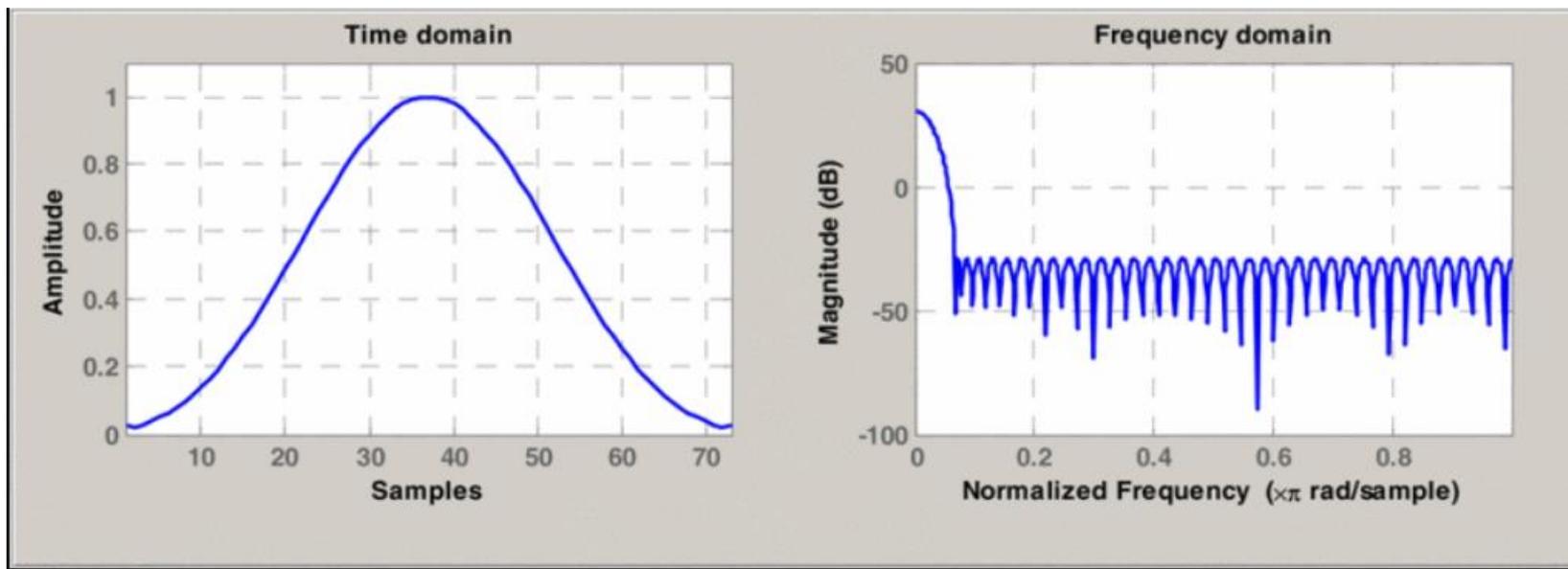
$$w(n) = w_0(n - (N-1)/2), \quad 0 \leq n \leq N-1$$

Universal Filtered Multi-Carrier (UFMC) (3/5)

- ◆ Dolph–Chebychev filters are optimal in the sense that for a given side lobe level (SLL) the main lobe width is **minimized**. They are adjustable by the tuning parameter for the **side lobe attenuation (SLA)** as well as by the filter length L .
- ◆ For example, on the one hand, in high ICI use cases with asynchronous transmission, it makes sense to use filters which are longer than the guard interval $L > N_{GI}$, at the price of higher vulnerability to delay spreads .
- ◆ On the other hand, in environments with high delay spread, a shorter filter length is used to protect against ISI. The SLA controls the trade-off between the main lobe width and the SLL.

Universal Filtered Multi-Carrier (UFMC) (4/5)

The side lobes of the Dolph-Chebyshev window transform are equal height, they are often called “ripple in the stop-band”



Dolph-Chebyshev window ($L=73, \alpha_{SLA} = 60$ dB).

Universal Filtered Multi-Carrier (UFMC) (5/5)

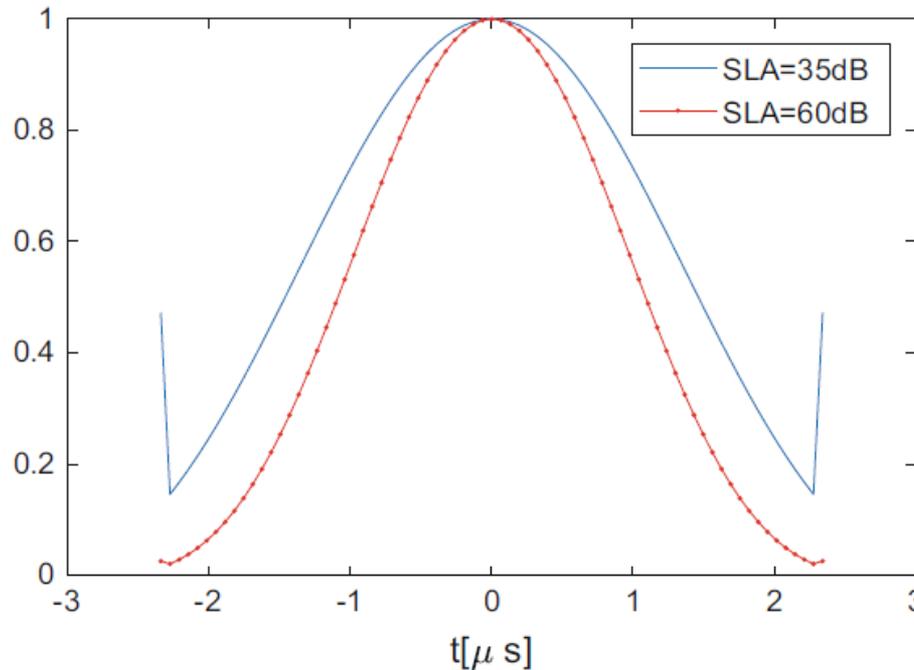


Fig. 2.11 Time domain impulse response for Dolph–Chebyshev filter with $L = 72$ and $SLA = 35, 60$ dB

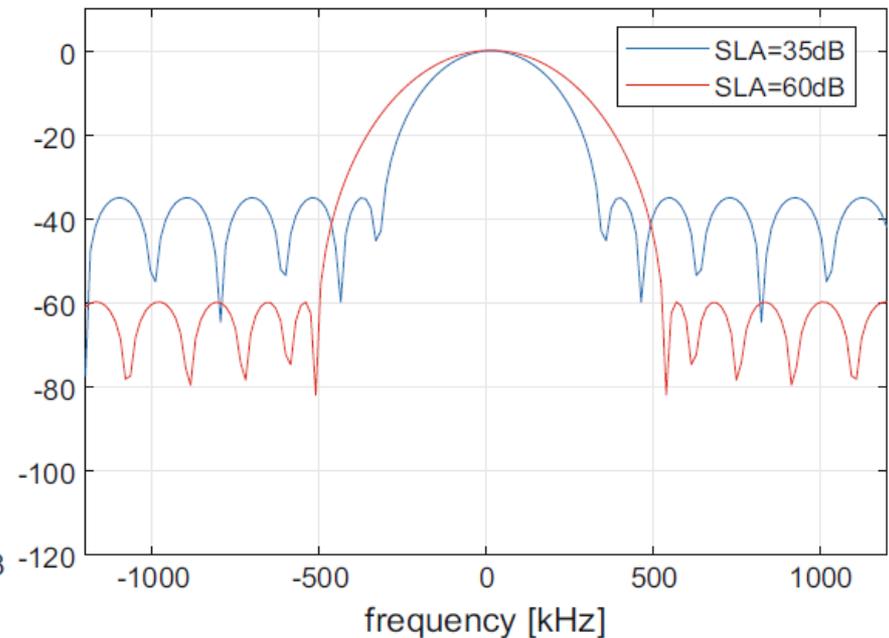
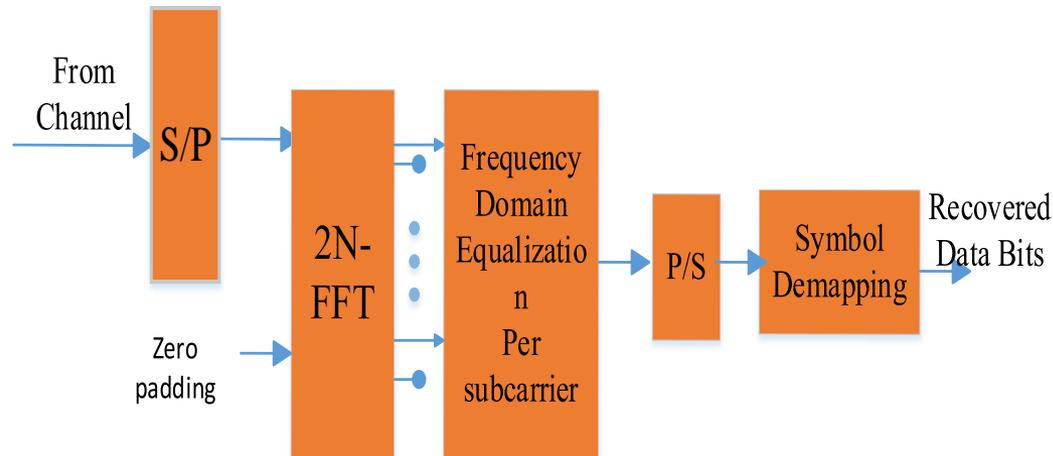
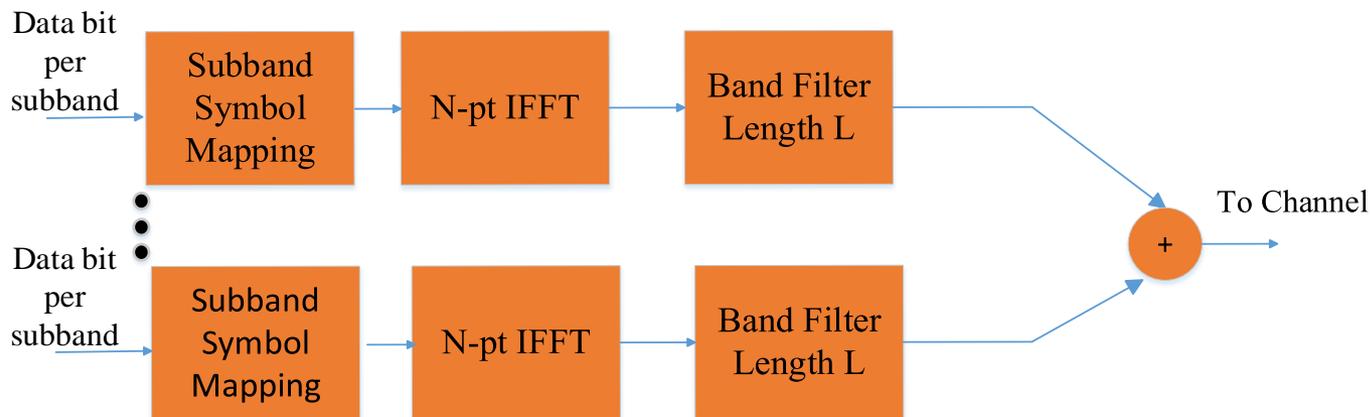


Fig. 2.12 Frequency domain response for Dolph–Chebyshev filter with $L = 72$ and $SLA = 35, 60$ dB

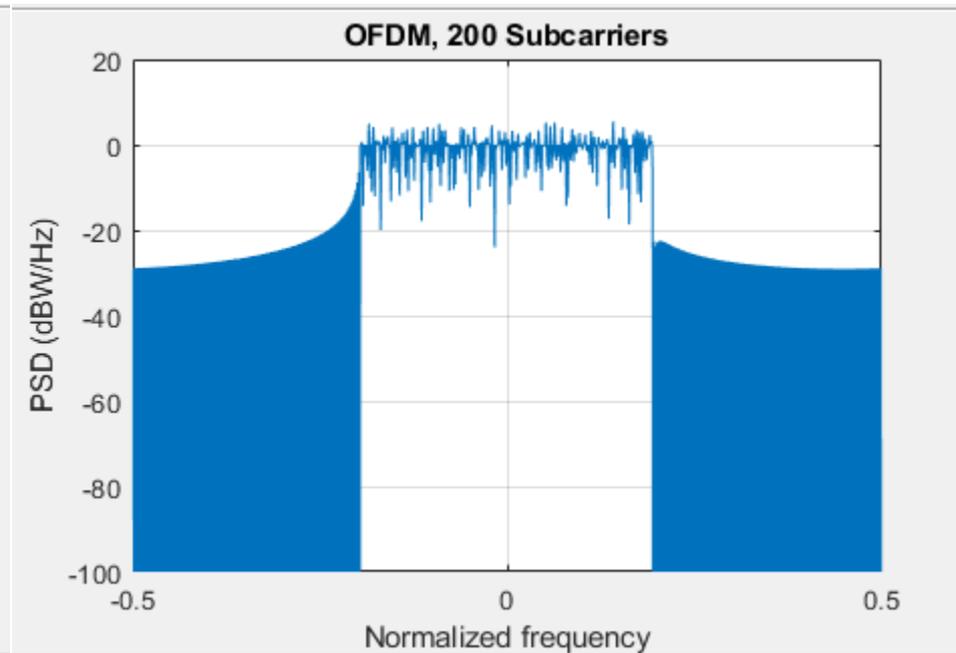
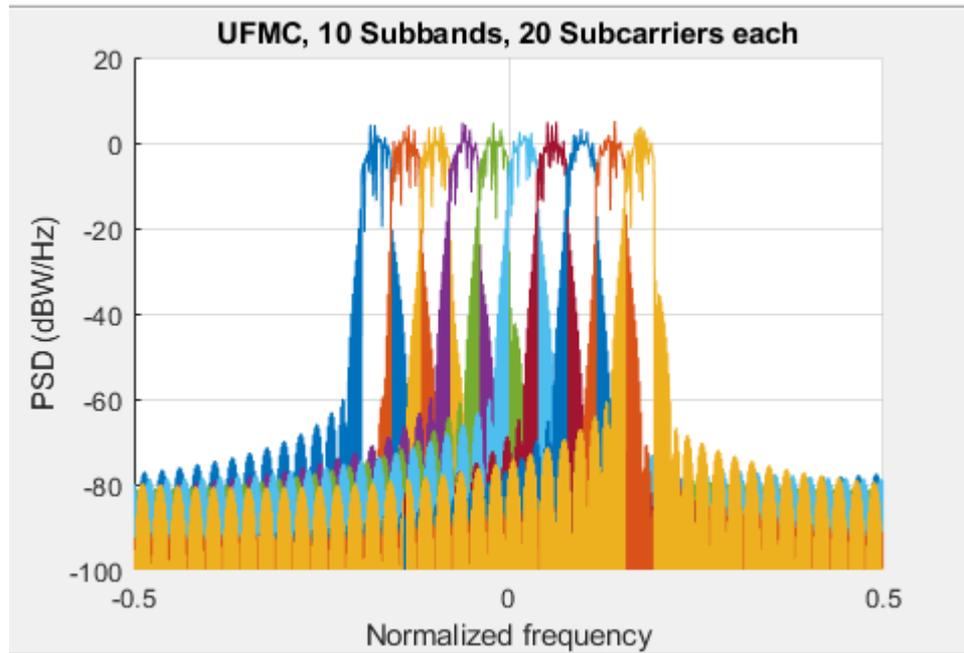
Matlab simulation (1/2)



| Simulation Parameter | Parameter Value |
|---|-----------------|
| UFMC system | |
| The number of subbands | 10 |
| The number of subcarrier in one subband | 20 |
| Subband Offset | 156 |
| Filter length | 43 |
| sidelobe attenuation | 40 |
| Size of IFFT | 512 |
| OFDM system | |
| The number of subcarriers | 200 |
| Subband Offset | 156 |
| Size of IFFT | 512 |

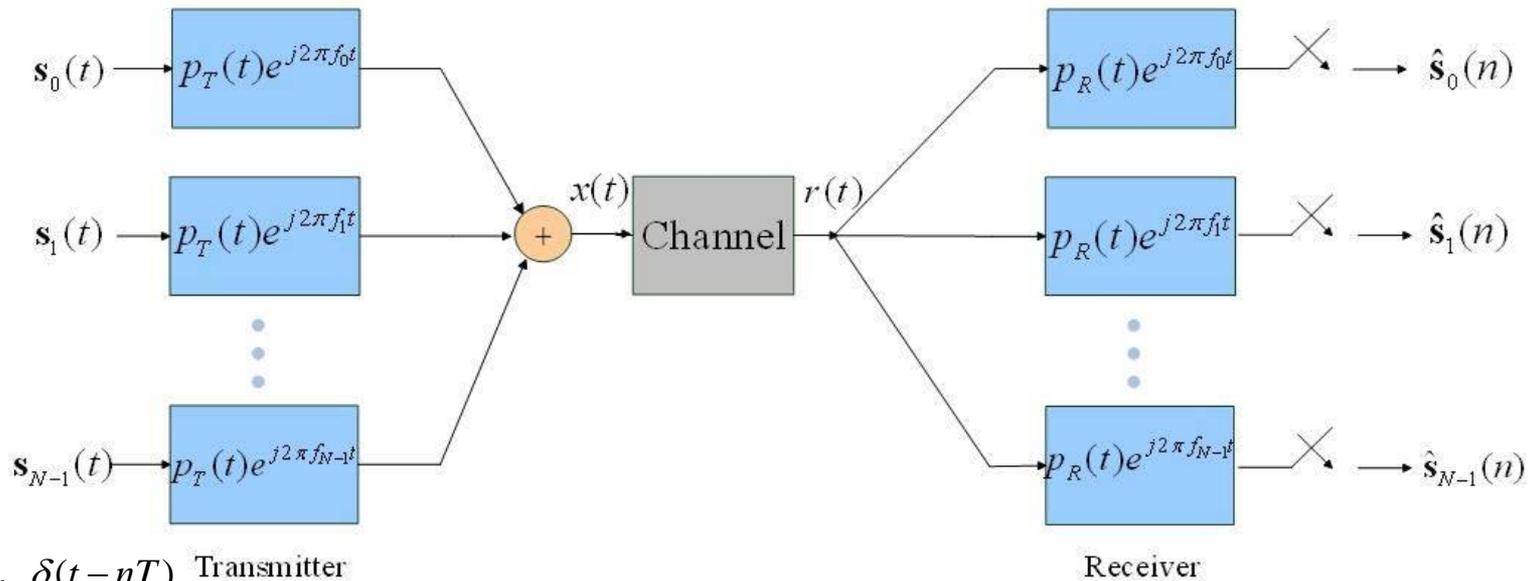
Matlab Simulation (2/2)

The PSD of UFMC and OFDM



The Filter Bank Multi-Carrier (FBMC) Waveform

FBMC System (1/3)



$$s_k(t) = \sum_n A_{k,n} \delta(t - nT) \quad \text{Transmitter}$$

- Mathematically, the transmitted signal, $x(t)$, of a multicarrier system in the time domain can be expressed as

$$x(t) = \sum_n \sum_{k=0}^{N-1} g_{k,n}(t) A_{k,n}$$

where $A_{k,n}$ denotes the transmitted symbol at subcarrier position k and time position n , and is chosen from a symbol alphabet, usually a QAM or a PAM signal constellation.

FBMC System (2/3)

- ◆ The basis pulse $g_{k,n}(t)$ is defined by

$$g_{k,n}(t) = p(t - nT)e^{j2\pi kF(t - nT)}$$

and is, essentially, a time and frequency shifted version of prototype filter $p(t)$, with T denoting the time spacing and F the frequency spacing (subcarrier spacing).

- ◆ After transmission over a channel, the received symbols are decoded by projecting the received signal, $r(t)$, onto the basis pulses, $g_{k,n}(t)$, that is,

$$y_{k,n} = \langle r(t), g_{k,n}(t) \rangle = \int_{-\infty}^{\infty} r(t) g_{k,n}^*(t) dt$$

FBMC System (3/3)

- ◆ Multicarrier systems are mainly characterized by prototype filter $p(t)$ as well as time spacing T and frequency spacing F , so that the ambiguity function,

$$A(\tau, \nu) = \int_{-\infty}^{\infty} p\left(t - \frac{\tau}{2}\right) p^*\left(t + \frac{\tau}{2}\right) e^{j2\pi\nu t} dt$$

captures the main properties of a multicarrier system in a compact way.

- ◆ The projection of the transmitted basis pulses $g_{k_1, n_1}(t)$ onto the received basis pulses $g_{k_2, n_2}(t)$ can then be expressed by the ambiguity function according to

$$\langle g_{k_1, n_1}(t), g_{k_2, n_2}(t) \rangle = e^{-j\pi TF(k_1+k_2)(n_1-n_2)} A(T(n_1-n_2), F(k_1-k_2))$$

only a phase shift
ambiguity function

Prototype Filter (1/3)

- ◆ There exist some fundamental limitations of multicarrier systems, as formulated by the Balian–Low theorem, which states that it is mathematically impossible that the following four desired properties are fulfilled at the same time [7]:

1. Maximum symbol density, $\frac{1}{TF} = 1$

2. Time-localization, $\sigma_t = \sqrt{\int_{-\infty}^{\infty} (t - \bar{t})^2 |p(t)|^2 dt} < \infty$

3. Frequency-localization, $\sigma_f = \sqrt{\int_{-\infty}^{\infty} (f - \bar{f})^2 |P(f)|^2 df} < \infty$

4. Orthogonality, $\langle g_{l_1, k_1}(t), g_{l_2, k_2}(t) \rangle = \delta_{(l_1 - l_2), (k_1 - k_2)}$
 $A(T(k_1 - k_2), F(l_1 - l_2)) = \delta_{(l_1 - l_2), (k_1 - k_2)}$



Prototype Filter (2/3)

| | Maximum symbol density | Time-localization | Frequency-localization | Orthogonality |
|--------------|------------------------|-------------------|------------------------|---------------|
| OFDM (no CP) | yes | yes | no | yes |
| FBMC/QAM | no | yes | yes | yes |
| FBMC/OQAM | yes | yes | yes | Real only |

Prototype Filter (3/3)

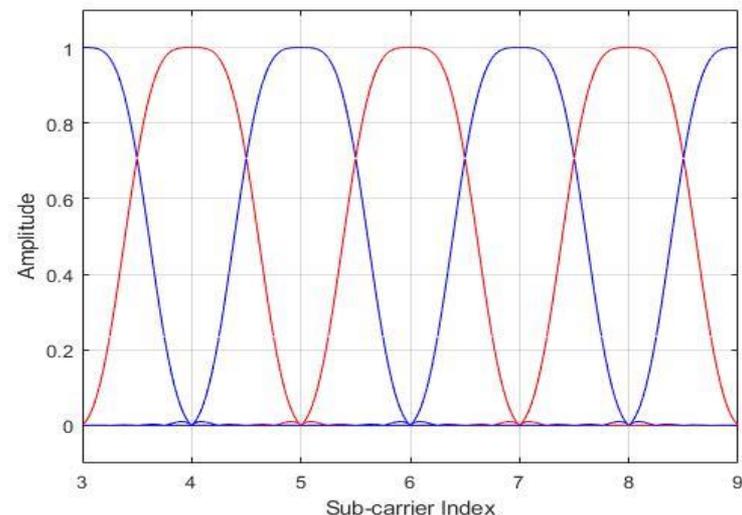
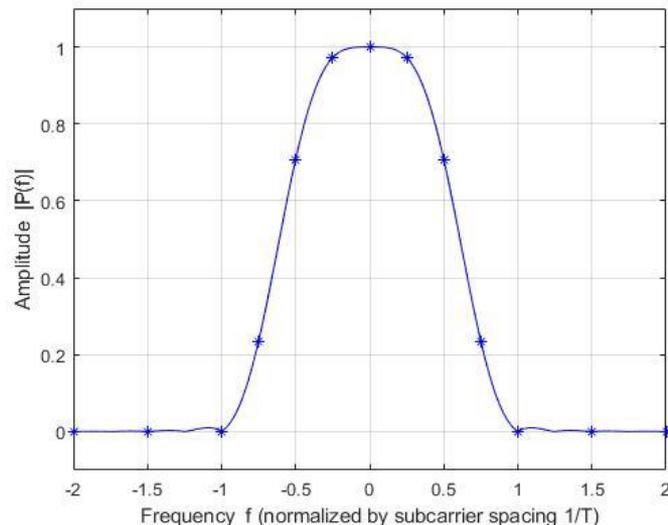
- ◆ A prominent filter is the **PHYDYAS** prototype filter [6]

$$P(f) = \sum_{k=-(K-1)}^{K-1} H_k \frac{\sin(\pi(f - \frac{k}{NK})NK)}{NK \sin(\pi(f - \frac{k}{NK}))}$$

| K | H ₀ | H ₁ | H ₂ | H ₃ | σ ² (dB) |
|---|----------------|----------------|----------------|----------------|---------------------|
| 2 | 1 | √2/2 | - | - | -35 |
| 3 | 1 | 0.911438 | 0.411438 | - | -44 |
| 4 | 1 | 0.971960 | √2/2 | 0.235147 | -65 |

Orthogonal: $T = T_0$; $F = 2/T_0 \rightarrow TF = 2$

Localization: $\sigma_t = 0.2745T_0$; $\sigma_f = 0.328/T_0$

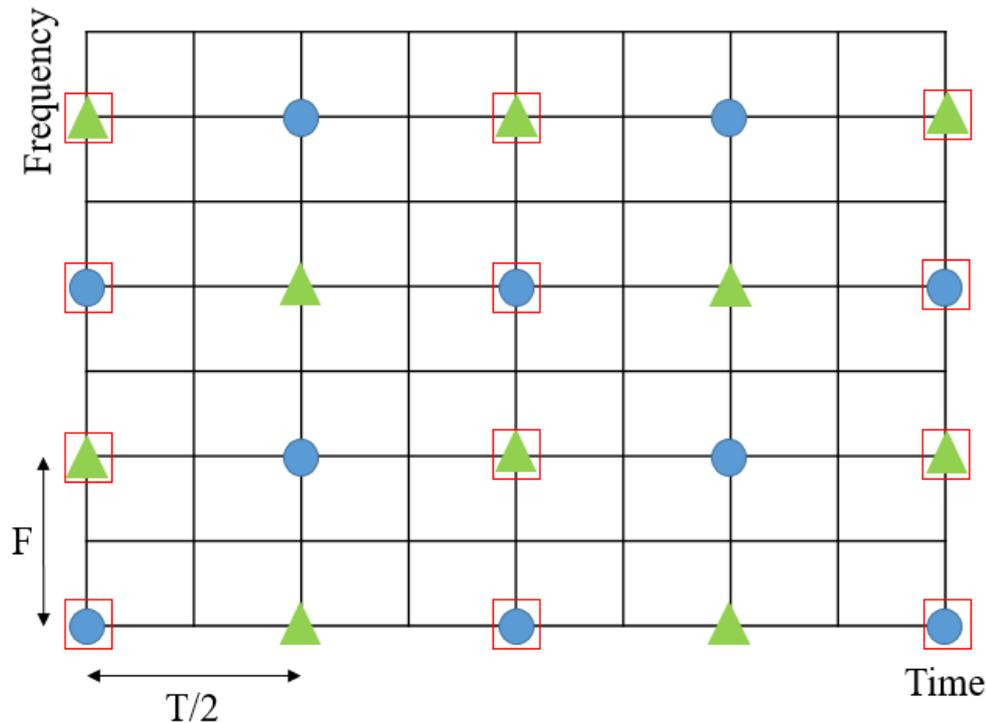




Offset QAM (OQAM) (1/2)

- ◆ In FBMC systems, any kind of modulation can be used, whenever the sub-channels are separated.
- ◆ For example, if only the sub-channels with even (odd) index are exploited, there is no overlap and QAM modulation can be employed.
- ◆ However, if full speed is sought, all the sub-channels must be exploited and a specific modulation is needed to cope with the frequency domain overlapping of the neighbouring sub-channels.
- ◆ Then, the strategy to reach full capacity is the following:
 - Double the symbol rate and, for each sub-channel, use alternatively the real and the imaginary part of the iFFT.
 - This way, the real and the imaginary part of a complex data symbol are not transmitted simultaneously as in OFDM, but the imaginary part is delayed by half the symbol duration.
- ◆ This is the so-called **offset quadrature amplitude modulation (OQAM)** and the term ‘offset’ reflects the time shift of half the inverse of the sub-channel spacing between the real part and the imaginary part of a complex symbol.

Offset QAM (OQAM) (2/2)



- Real part
- ▲ Imaginary part
- Complex QAM symbol

$F = 1/T$: subcarrier spacing

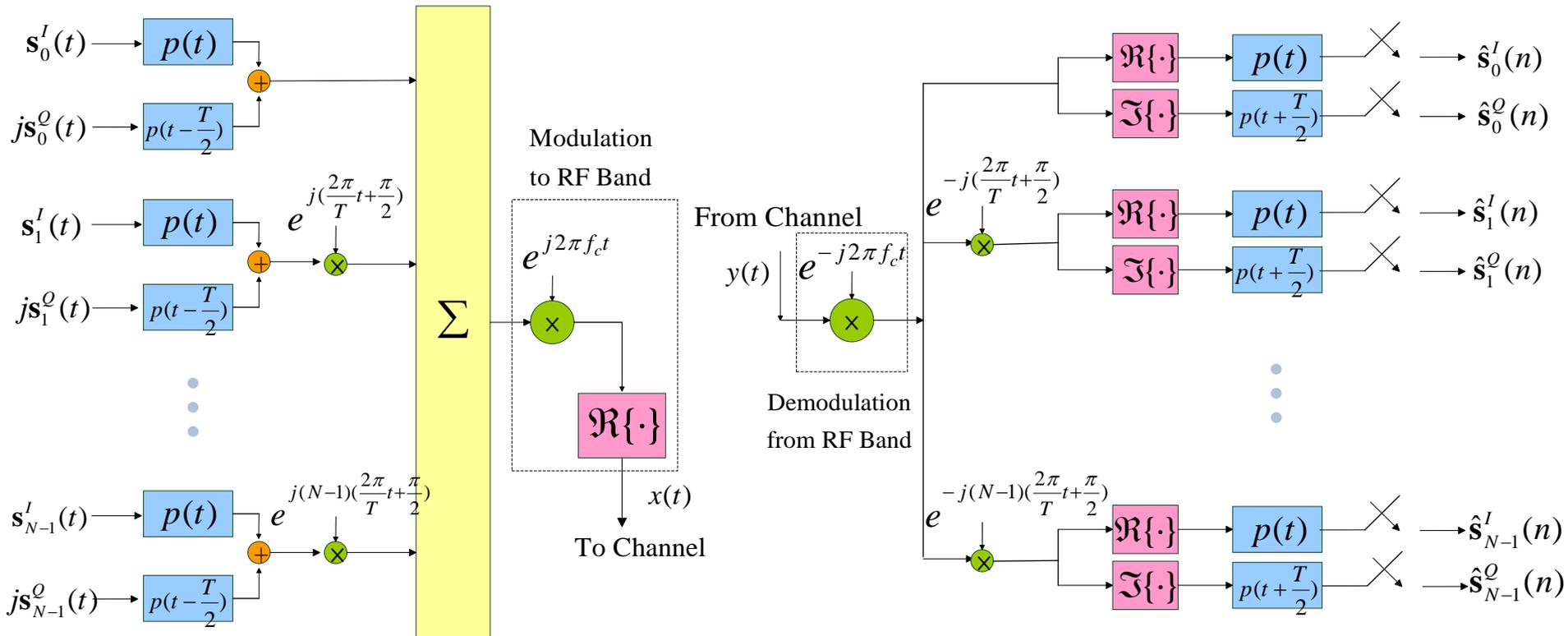
T : OFDM/QAM symbol duration

Symbol density

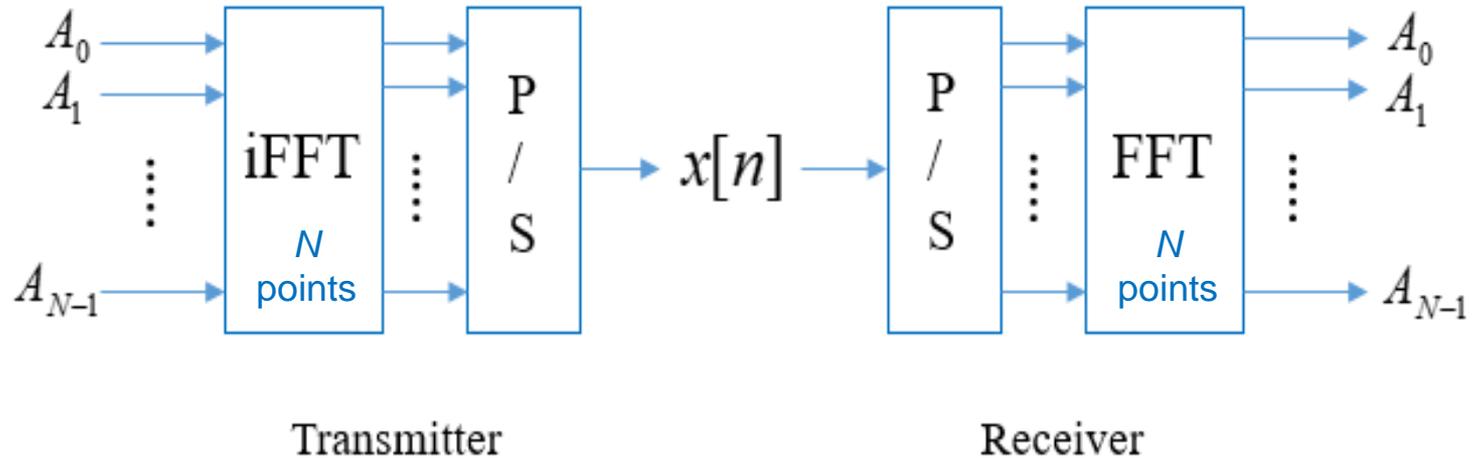
OFDM/QAM (without CP) : $1/TF = 1$

FBMC/OQAM : $\frac{1}{(T/2)F} = 2 \Rightarrow 1$ (complex)

FBMC/OQAM System



Fast Fourier Transform Architecture (1/2)

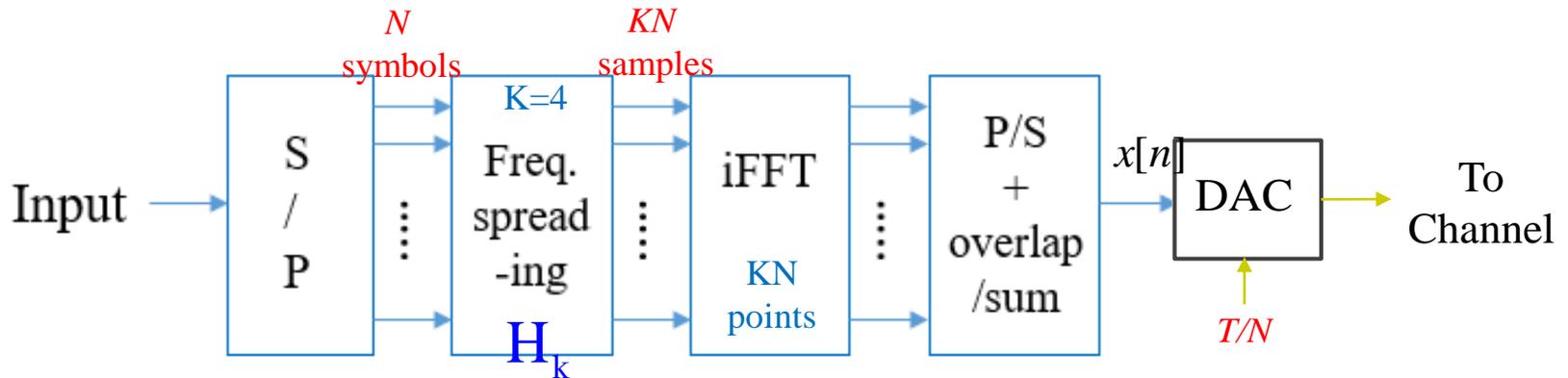


- ◆ In the presence of a channel with **multipath propagation**, due to the channel impulse response, the multicarrier symbols overlap at the receiver input and it is no more possible to demodulate with just the FFT, because inter-symbol interference has been introduced and the orthogonality property of the carriers has been lost.

Fast Fourier Transform Architecture (2/2)

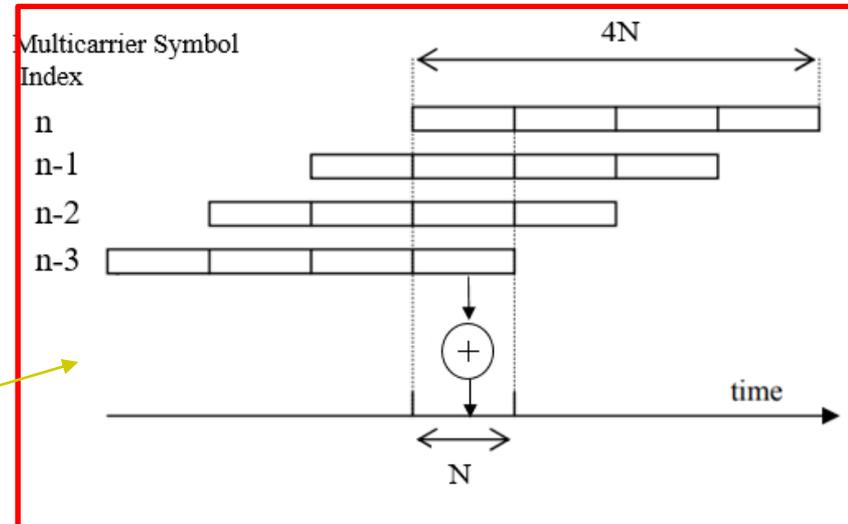
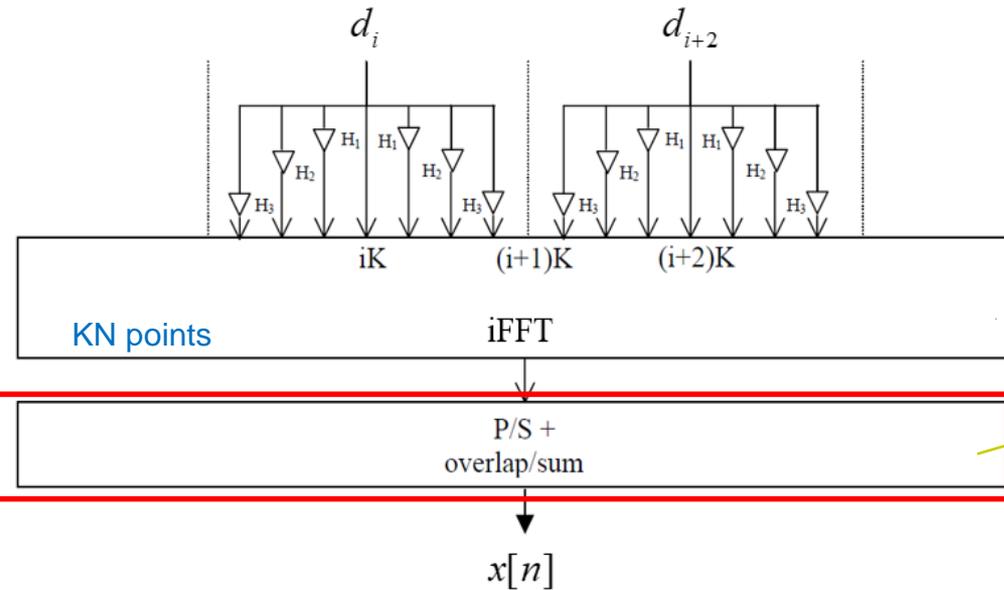
1. Extend the symbol duration by a guard time exceeding the length of the channel impulse response and still demodulate with the same FFT. The scheme is called **OFDM**.
2. Keep the timing and the symbol duration as they are, but add some processing to the FFT. The scheme is called **FBMC**, because this additional processing and the FFT together constitute **a bank of filters**.

Extended FFT Method (1/3)



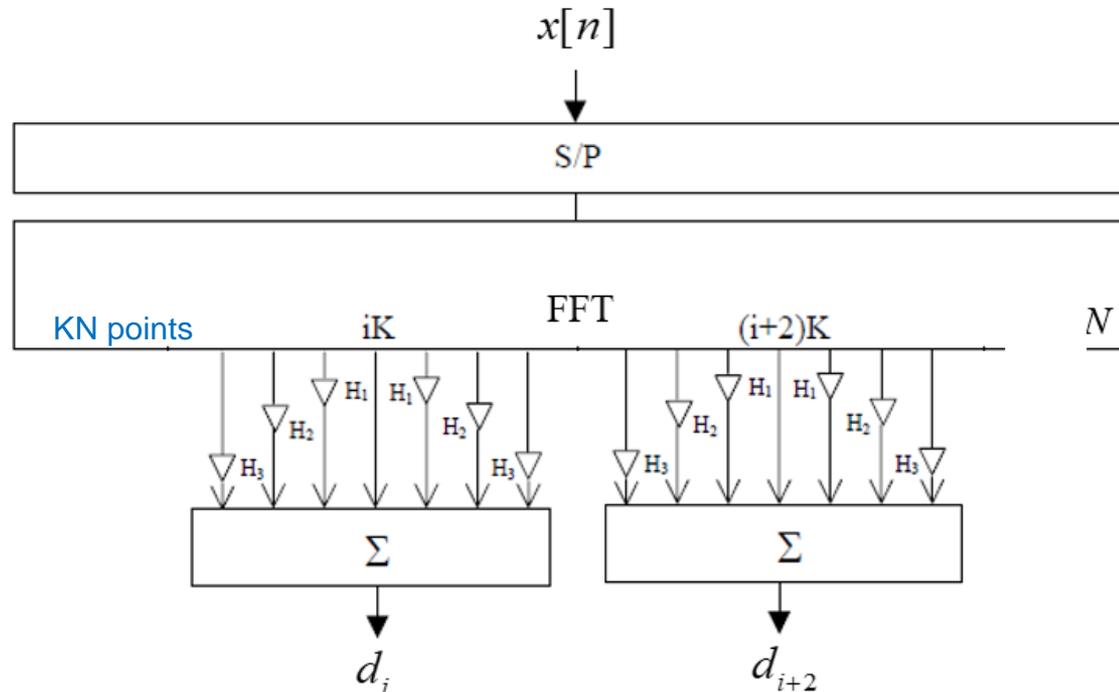
- ◆ The filter bank in the transmitter can be implemented as follows
 - an iFFT of size KN is used, to generate all the necessary carriers,
 - a particular data element after multiplication by the filter frequency coefficients, is fed to the $2K-1$ inputs of the iFFT.
 - Practically, the data element is spread over several iFFT inputs and the operation can be called “**weighted frequency spreading**”.

Extended FFT Method (2/3)



| K | H ₀ | H ₁ | H ₂ | H ₃ | σ ² (dB) |
|---|----------------|----------------|----------------|----------------|---------------------|
| 2 | 1 | √2/2 | - | - | -35 |
| 3 | 1 | 0.911438 | 0.411438 | - | -44 |
| 4 | 1 | 0.971960 | √2/2 | 0.235147 | -65 |

Extended FFT Method (3/3)



- ◆ The implementation of the receiver is based on an extended FFT of size KN .
- ◆ At the output of the FFT, the data elements are recovered with the help of a weighted despreading operation.
- ◆ In fact, the data recovery rests on the following property of the frequency coefficients of the Nyquist filter $\frac{1}{K} \sum_{k=-K+1}^{K-1} |H_k|^2 = 1$

Matlab Simulation

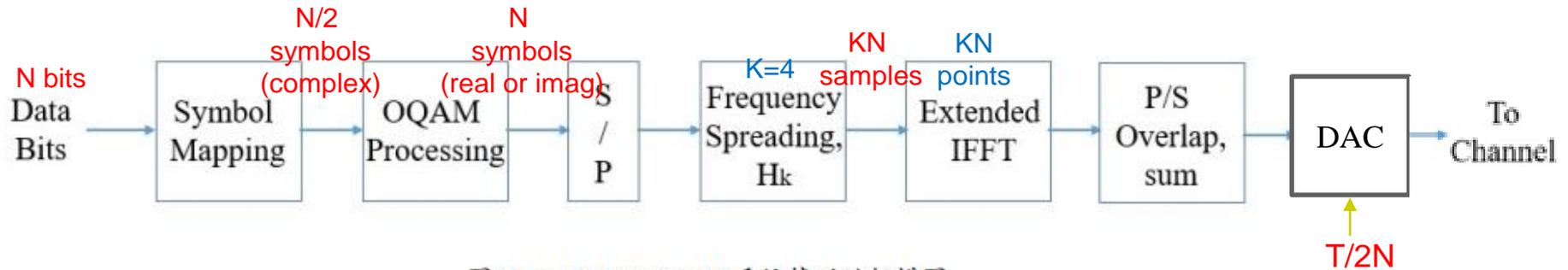


圖 31: FBMC/OQAM 系統傳送端架構圖

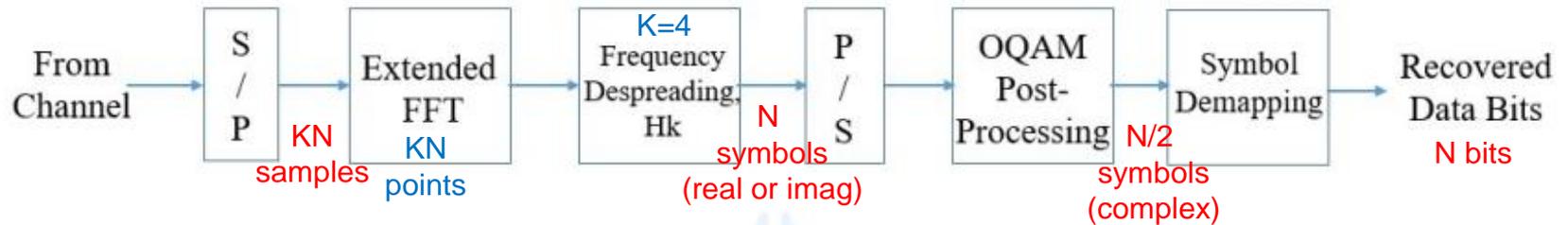
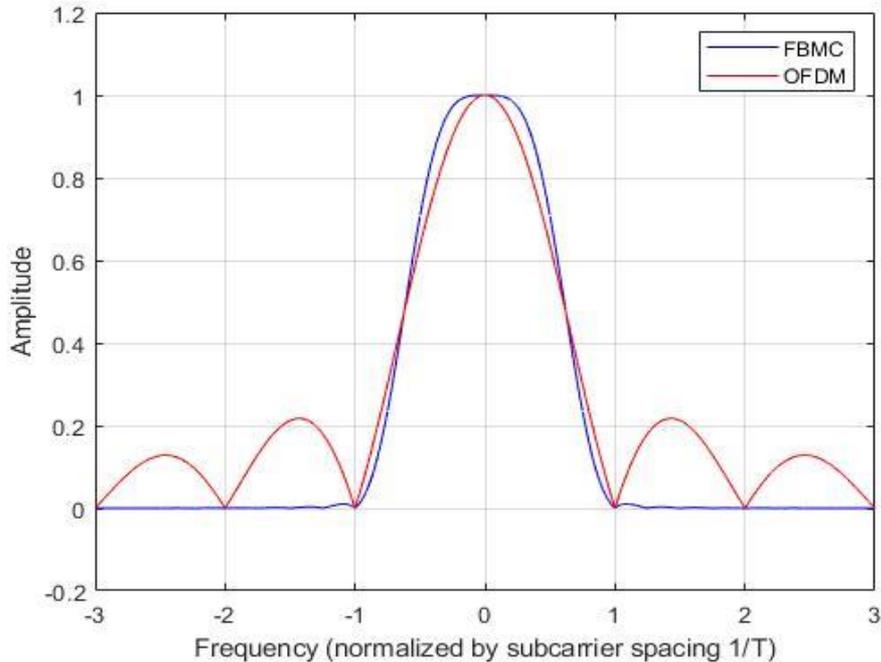


圖 34: FBMC/OQAM 系統接收端架構圖

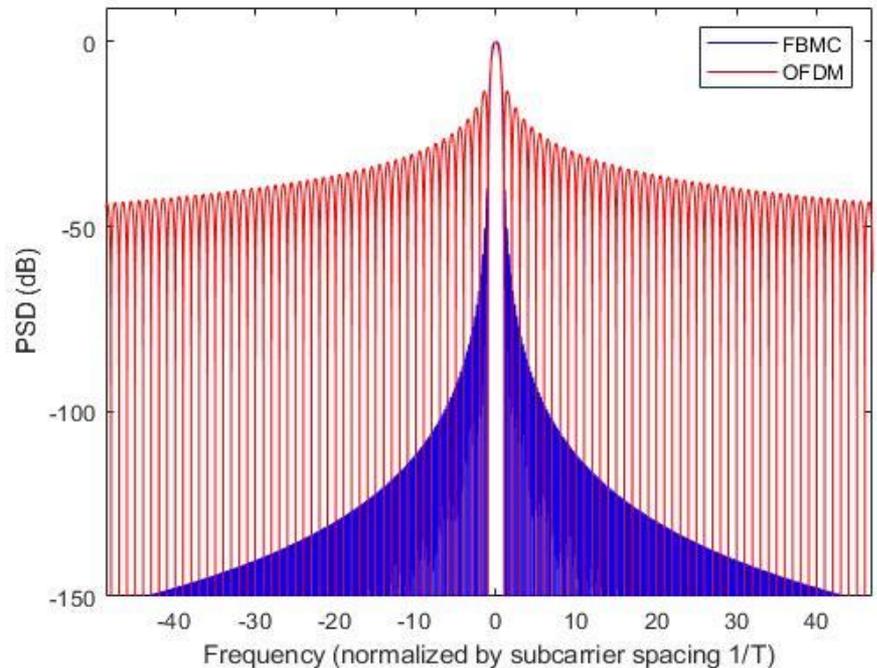
| | OFDM (no CP) | FBMC |
|-------------------------------|--------------|----------------------|
| Number of subcarriers (N) | 1024 | 1024 |
| Number of data subcarriers | 600 | 600 |
| Guard bands on both sides | 212 | 212 |
| Constellation mapping | 4-QAM | 4-OQAM |
| Overlapping factor K | - | 4 |
| FFT size | 1024 (N) | 4096 ($K \cdot N$) |

Mathworks. FBMC vs. OFDM Modulation - MATLAB & Simulink Example, June 2017.
[Online] Available: https://ww2.mathworks.cn/help/comm/examples/fbmc-vs-ofdm-modulation.html?s_tid=srchtitle

Prototype Filter

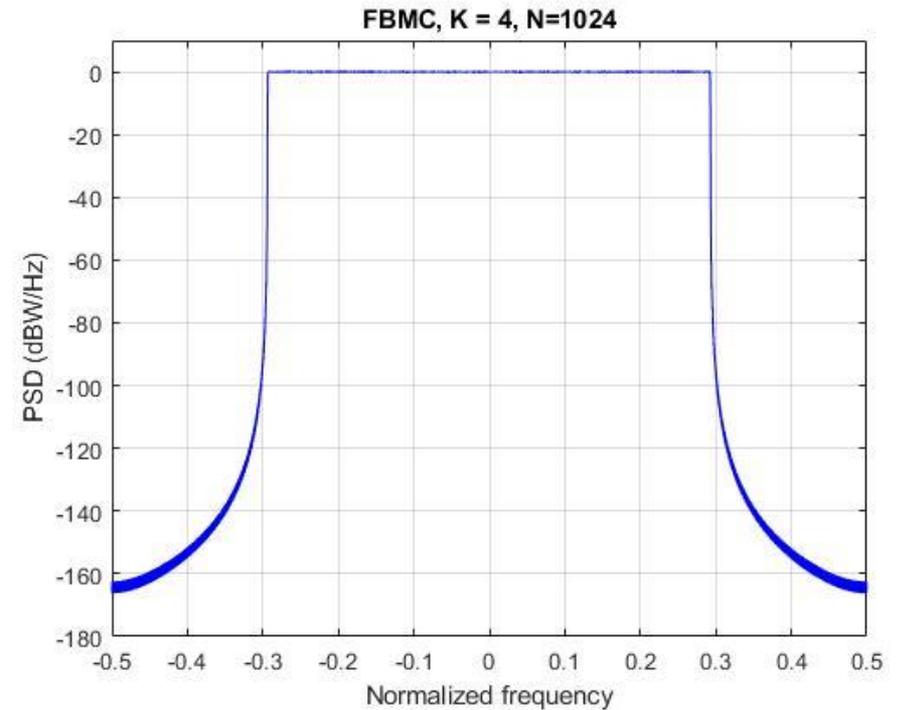
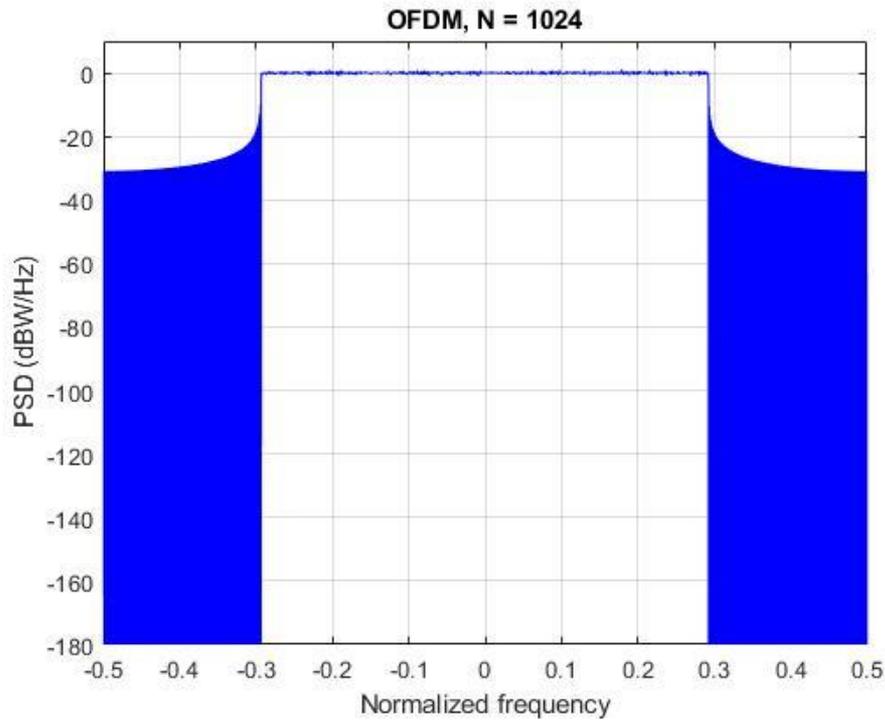


Frequency responses of the prototype filters of **OFDM** and **FBMC** (PHYDYAS filter, $K=4$).



Comparison of spectrum of **OFDM** and **FBMC** (PHYDYAS filter, $K=4$) for one subcarrier.

Power Spectral Density



Error Rate Analysis (1/2)

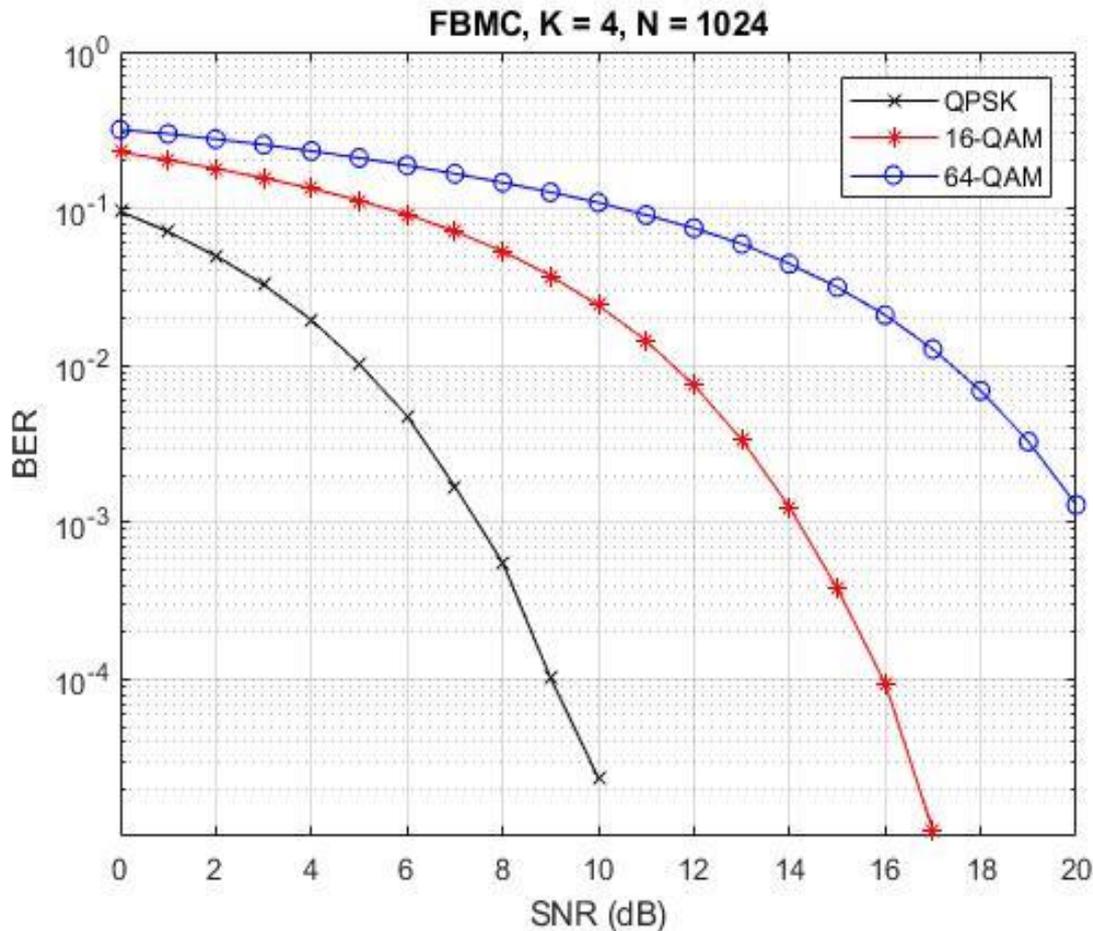


圖 35: FBMC/OQAM 系統在不同調變下的錯誤率比較 (AWGN channel)

Error Rate Analysis (2/2)

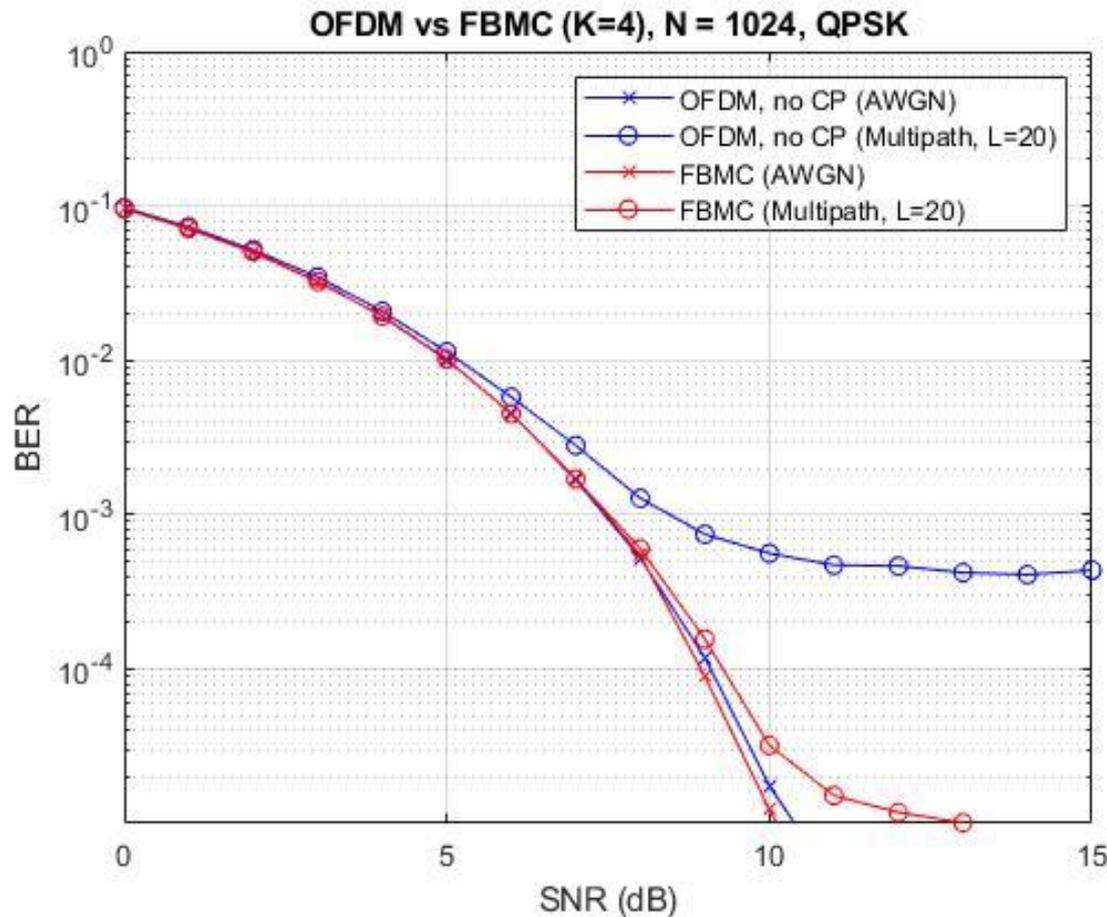


圖 36: 比較OFDM (未加CP) 及FBMC/OQAM 系統在多路徑通道效應下的差異

The Generalized Frequency Division Multiplexing (GFDM) Waveform

The GFDM System

- ◆ GFDM arranges the data symbols in a time-frequency grid, consisting of M subsymbols and K subcarriers, and applies a circular prototype filter for each subcarrier[13].
- ◆ The total number of symbols follows as $N=KM$.

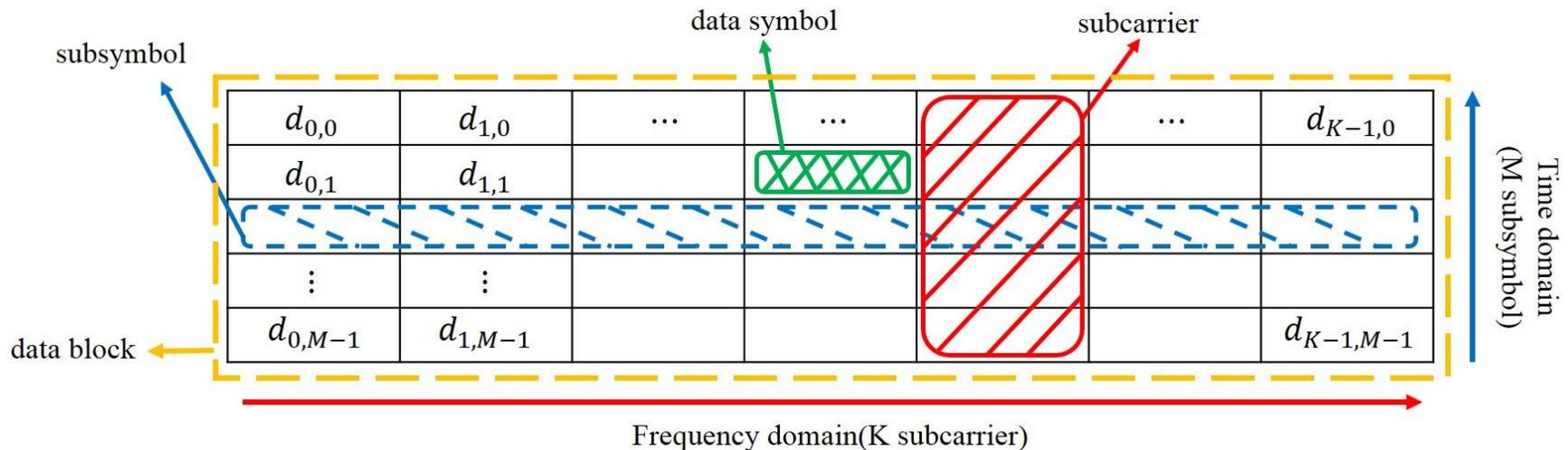
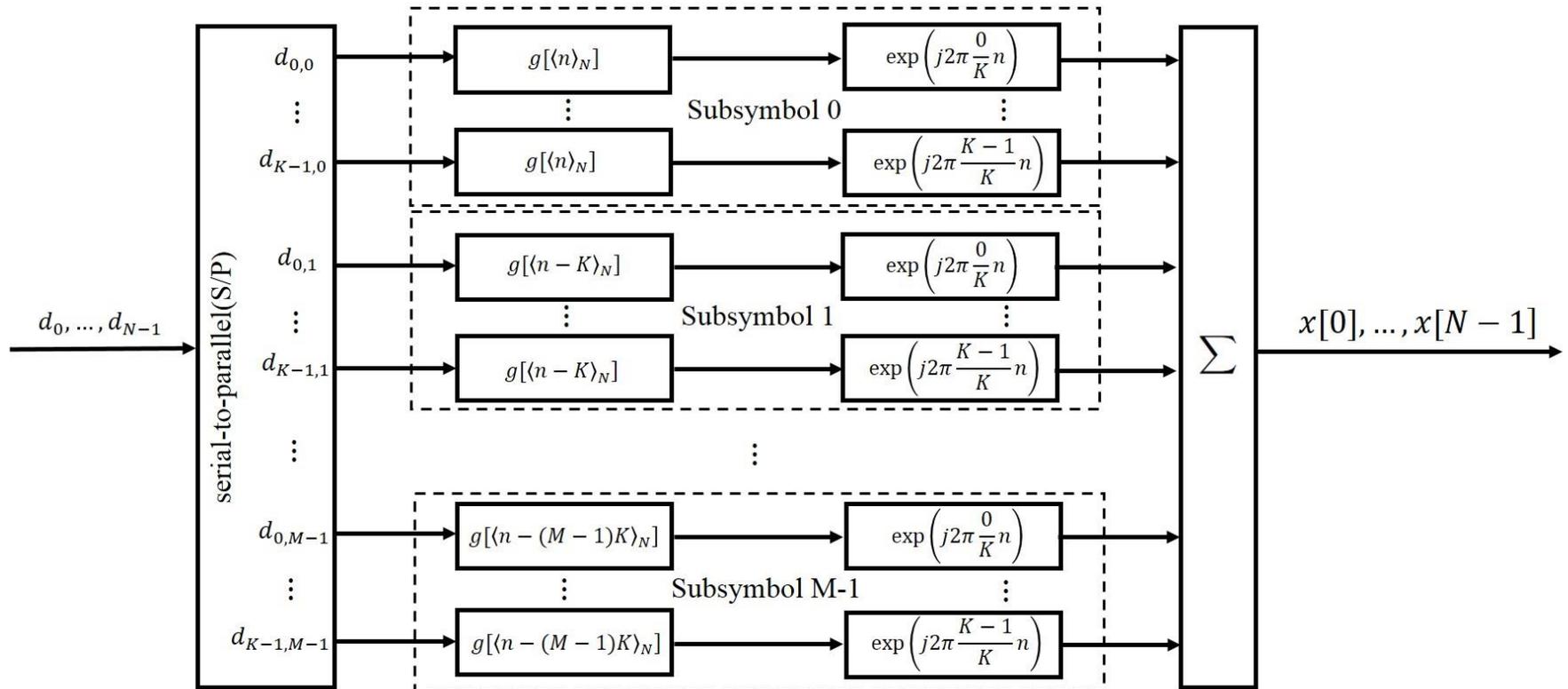


Fig 1: Overview of block structure and terminology

[13] G.Fettweis, M. Krondorf, and S. Bittner, "GFDM – generalized frequency division multiplexing," in *Proc. 69th IEEE Vehicular Technology Conference (VTC), Barcelona, Spain, April. 2009*, pp.1-4.

GFDM Modulator (1/4)



GFDM Modulator (2/4)

Each $d_{k,m}$ is transmitted with the corresponding pulse shape [14]

$$g_{k,m}[n] = g[\langle n - mK \rangle_N] \cdot \exp\left(-j2\pi \frac{k}{K} n\right)$$

With $n = 0, 1, \dots, N - 1$ denoting the sampling index.

Each $g_{k,m}[n]$ is a time and frequency shifted version of a prototype filter $g[n]$, the filter on different sub-symbols as

$$g[\langle n - mK \rangle_N] = \delta[\langle n - mK \rangle_N] \otimes g[n]$$

where \otimes is the circular convolution.

The data symbols as

$$\mathbf{d} = \left(d_{0,0}, d_{1,0}, \dots, d_{K-1,0}, d_{0,1}, \dots, d_{K-1,1}, \dots, d_{0,M-1}, \dots, d_{K-1,M-1} \right)^T$$

[14] N. Michailow, M. Matthé, I. Gaspar, A. Caldevilla, L. Mendes, A. Festag, and G. Fettweis, "Generalized frequency division multiplexing for 5th generation cellular networks," *IEEE Trans. On Commun.*, vol. 62, no. 9, pp. 1-17, Sep. 2014.

GFDM Modulator (3/4)

Explain from a series of modulations in Fig 2, the GFDM transmit samples $\mathbf{x} = (x[n])^T$ are obtained by superposition of all transmit symbols

$$\begin{aligned}
 x[n] &= \sum_{k=0}^{K-1} \sum_{m=0}^{M-1} g[\langle n - mK \rangle_N] \cdot \exp\left(-j2\pi \frac{k}{K} n\right) d_{k,m} \\
 &= \sum_{k=0}^{K-1} \sum_{m=0}^{M-1} \mathbf{g}_{k,m}[n] d_{k,m}
 \end{aligned} \tag{1}$$

Collecting the filter samples in a vector $\mathbf{g}_{k,m} = (g_{k,m}[n])^T$ allows to formulate (1) as

$$\mathbf{x} = \left[\mathbf{g}_{0,0}, \mathbf{g}_{1,0}, \dots, \mathbf{g}_{K-1,0}, \mathbf{g}_{0,1}, \dots, \mathbf{g}_{K-1,M-1} \right]_{N \times N} \begin{bmatrix} d_{0,0} \\ d_{1,0} \\ \vdots \\ d_{K-1,0} \\ d_{0,1} \\ \vdots \\ d_{K-1,M-1} \end{bmatrix}_{N \times 1}$$

GFDM Modulator (4/4)

And allows to formulate (1) as

$$\mathbf{x} = \mathbf{A}\mathbf{d}$$

Where \mathbf{A} is a $KM \times KM$ transmitter matrix [15].

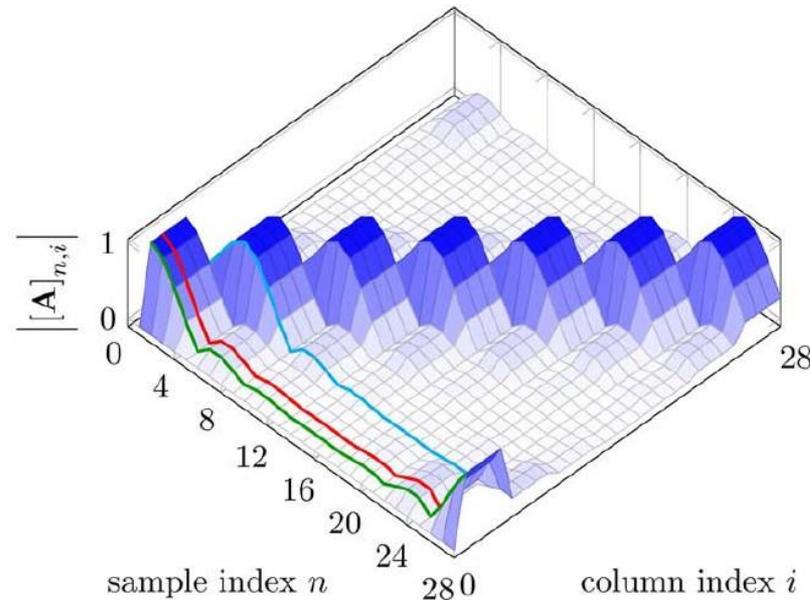


Fig 3: Illustration of GFDM transmitter matrix for $N=28$, $K=4$, $M=7$ and RC filter roll off factor = 0.4.

[15] N. Michailow, S. Krone, M. Lentmaier, G. Fettweis, "Bit Error Rate Performance of Generalized Frequency Division Multiplexing," in *IEEE Vehicular Technology Conference*, Sep. 2012, pp. 1-5.

Cyclic Prefix

| | | | | | | |
|-------------------|-------------|-------------------|-------------|-----|-------------------|---------------|
| Cyclic Prefix(CP) | $x_{0,0}$ | Cyclic Prefix(CP) | $x_{0,1}$ | ... | Cyclic Prefix(CP) | $x_{0,M-1}$ |
| | $x_{1,0}$ | | $x_{1,1}$ | | | $x_{1,M-1}$ |
| | $x_{2,0}$ | | $x_{2,1}$ | | | $x_{2,M-1}$ |
| | ⋮ | | ⋮ | | | ⋮ |
| | $x_{K-1,0}$ | | $x_{K-1,1}$ | | | $x_{K-1,M-1}$ |

(a) OFDM 訊號

| | | | | |
|-------------------|-------------|-------------|-----|---------------|
| Cyclic Prefix(CP) | $x_{0,0}$ | $x_{0,1}$ | ... | $x_{0,M-1}$ |
| | $x_{1,0}$ | $x_{1,1}$ | | $x_{1,M-1}$ |
| | $x_{2,0}$ | $x_{2,1}$ | | $x_{2,M-1}$ |
| | ⋮ | ⋮ | | ⋮ |
| | $x_{K-1,0}$ | $x_{K-1,1}$ | | $x_{K-1,M-1}$ |

(b) GFDM 訊號

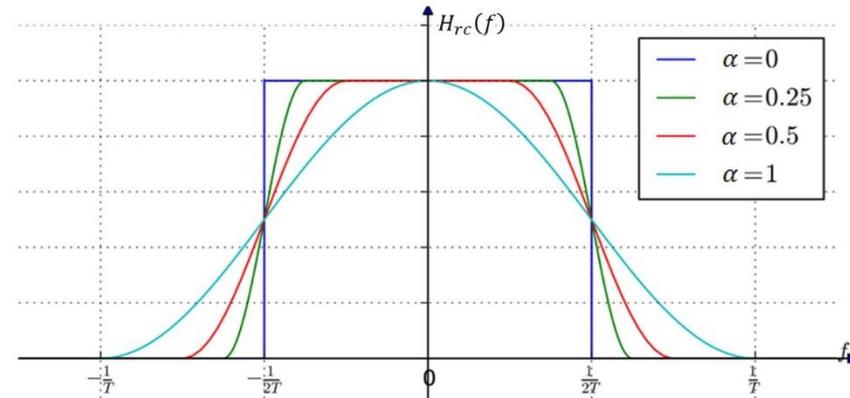
[16] B. Farhang-Boroujeny, and H. Moradi, "Derivation of GFDM based on OFDM principles," in *Proc. IEEE International Conference Communications(ICC)*, Jun. 2015, pp. 2680-2685.

Prototype Filter

Raised-cosine filter

$$H_{rc}(f) = \begin{cases} 1, & |f| \leq \frac{1-\alpha}{2T} \\ \frac{1}{2} \left[1 + \cos \left(\frac{\pi T}{\alpha} \left[|f| - \frac{1-\alpha}{2T} \right] \right) \right], & \frac{1-\alpha}{2T} < |f| \leq \frac{1+\alpha}{2T} \\ 0, & \text{otherwise} \end{cases}$$

$$h_{rc}(t) = \begin{cases} \frac{\pi}{4T} \operatorname{sinc} \left(\frac{1}{2\alpha} \right), & t = \pm \frac{T}{2\alpha} \\ \frac{1}{T} \operatorname{sinc} \left(\frac{t}{T} \right) \frac{\cos \left(\frac{\pi \alpha t}{T} \right)}{1 - \left(\frac{2\alpha t}{T} \right)^2}, & \text{otherwise} \end{cases}$$



Square-root-raised-cosine filter

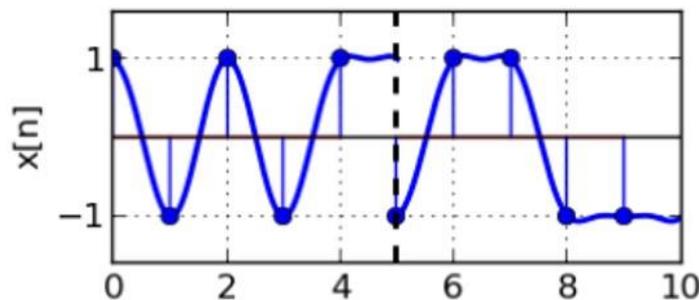
$$h_{srrc}(t) = \begin{cases} \frac{1}{T} \left(1 + \alpha \left(\frac{4}{\pi} - 1 \right) \right), & t = 0 \\ \frac{\alpha}{T\sqrt{2}} \left[\left(1 + \frac{2}{\pi} \right) \sin \left(\frac{\pi}{4\alpha} \right) + \left(1 - \frac{2}{\pi} \right) \cos \left(\frac{\pi}{4\alpha} \right) \right], & t = \pm \frac{T}{4\alpha} \\ \frac{1}{T} \frac{\sin \left[\pi \frac{t}{T} (1-\alpha) \right] + 4\alpha \frac{t}{T} \cos \left[\pi \frac{t}{T} (1+\alpha) \right]}{\pi \frac{t}{T} \left[1 - \left(4\alpha \frac{t}{T} \right)^2 \right]}, & \text{otherwise} \end{cases}$$

where T is the symbol period, and α is roll-off factor.

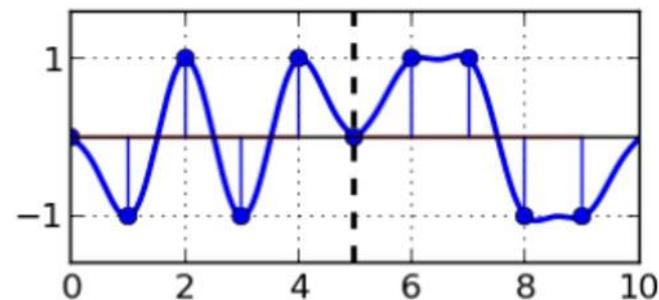
Guard Symbol Insertion

For the spectrum of the GFDM signal not only the pulse shaping but also the transition between subsequent blocks is important, since an abrupt change of the signal between two blocks creates a high OOB radiation.

In order to achieve more smooth transitions, a guard symbol can be inserted into each block, which means that $d_{k,0} = 0$ for all subcarriers [20].



(a) No guard symbol



(b) One guard symbol

[20] M. Matthé, N. Michailow, I. Gaspar, and G. Fettweis, "Influence of pulse shaping on bit error rate performance and out of band radiation of generalized frequency division multiplexing," in *IEEE International Conference Communications Workshops (ICC)*, June. 2014, pp. 43-48

GFDM Receiver

The overall transceiver equation can be written as

$$\mathbf{y} = \mathbf{H}\mathbf{x} + \mathbf{w}$$

Introducing as the received signal after channel equalization.

$$\begin{aligned}\mathbf{z} &= \mathbf{H}^{-1}\mathbf{H}\mathbf{x} + \mathbf{H}^{-1}\mathbf{w} \\ &= \mathbf{A}\mathbf{d} + \mathbf{H}^{-1}\mathbf{w}\end{aligned}$$

Linear demodulation of the signal can be expressed as

$$\hat{\mathbf{d}} = \mathbf{B}\mathbf{z}$$

Where \mathbf{B} is a $KM \times KM$ receiver matrix.

[14] N. Michailow, M. Matthé, I. Gaspar, A. Caldevilla, L. Mendes, A. Festag, and G. Fettweis, "Generalized frequency division multiplexing for 5th generation cellular networks," *IEEE Trans. On Commun.*, vol. 62, no. 9, pp. 1-17, Sep. 2014.

Several Receivers

The matched filter (MF) receiver maximizes the signal-to-noise ratio (SNR) per subcarrier, but with the effect of introducing self-interference when a non-orthogonal transmit pulse is applied.

$$\mathbf{B}_{MF} = \mathbf{A}^H$$

The zero-forcing (ZF) receiver on the contrary completely removes any self-interference at the cost of enhancing the noise.

$$\mathbf{B}_{ZF} = \mathbf{A}^{-1}$$

The linear minimum mean square error (MMSE) receiver

$$\mathbf{B}_{MMSE} = \left(\mathbf{R}_w^2 + \mathbf{A}^H \mathbf{H}^H \mathbf{H} \mathbf{A} \right)^{-1} \mathbf{A}^H \mathbf{H}^H$$

makes a trade-off between self-interference and noise enhancement.

[14] N. Michailow, M. Matthé, I. Gaspar, A. Caldevilla, L. Mendes, A. Festag, and G. Fettweis, "Generalized frequency division multiplexing for 5th generation cellular networks," *IEEE Trans. On Commun.*, vol. 62, no. 9, pp. 1-17, Sep. 2014.